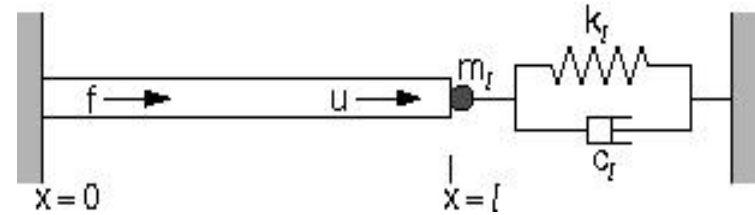
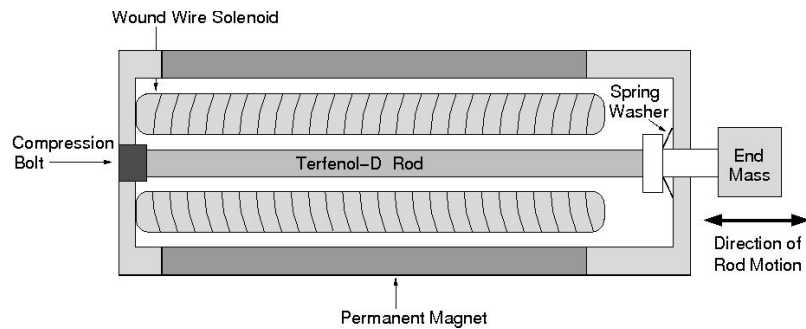


# Development and Approximation of Rod Models

“He has Van Gogh’s ear for music,” Billy Wilder

# Motivation: Terfenol-D Transducer



## Questions:

- Are inputs uniform along rod length?
- How can this be determined?
- What magnetomechanical behavior must be incorporated in models?

# Uniform Inputs: Spring Model

**Spring Model:** Consider magnetic field inputs  $H(t)$

$$m \frac{d^2 u}{dt^2} + c \frac{du}{dt} + ku = a_2 M^2(H(t))$$

$$u(t_0) = u_0$$

$$\frac{du}{dt}(t_0) = u_1$$

**Questions:**

- Can we compute an analytic solution?
- What numerical techniques can we use?
- How do we know if numerical techniques are converged?

**Note:**

- Appropriate analytic and numerical techniques will depend, in part, on nature of  $M(H)$ .

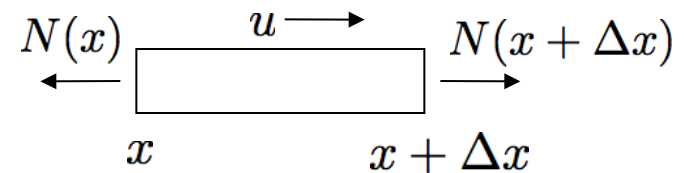
# Nonuniform Inputs: Rod Model

Force Balance:

$$\int_x^{x+\Delta x} \rho A \frac{\partial^2 u}{\partial t^2}(t, s) ds = N(t, x + \Delta x) - N(t, x) + \int_x^{x+\Delta x} f(t, s) ds$$

Strategy: Multiply by  $\frac{1}{\Delta x}$  and take limit to get

$$\rho A \frac{\partial^2 u}{\partial t^2} = \frac{\partial N}{\partial x} + f$$



Note:  $N = \sigma A$  ,  $\varepsilon = \lim_{\Delta x \rightarrow 0} \frac{\Delta u}{\Delta x} = \frac{\partial u}{\partial x}$

Constitutive Relations:

$$\sigma = Y\varepsilon + c \frac{\partial \varepsilon}{\partial t} - a_2 M^2(H)$$

$$M(H) = \int_0^\infty \int_{-\infty}^\infty \mu(H_c, H_I) \overline{M}(H + H_I; H_c) dH_I dH_c$$

# Rod Model (Strong Formulation)

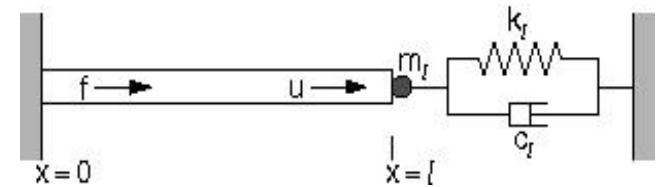
Rod Model:

$$\rho A \frac{\partial^2 u}{\partial t^2} - Y A \frac{\partial^2 u}{\partial x^2} - c A \frac{\partial^3 u}{\partial x^2 \partial t} = f - a_2 A \frac{\partial(M^2(t))}{\partial x}$$

Boundary Conditions:

$$u(t, 0) = 0$$

$$N(t, \ell) = -k_\ell u(t, \ell) - c_\ell \frac{\partial u}{\partial t}(t, \ell) - m_\ell \frac{\partial^2 u}{\partial t^2}(t, \ell)$$



Initial Conditions:

$$u(0, x) = u_0(x)$$

$$\frac{\partial u}{\partial t}(0, x) = u_1(x)$$

Issues:

# Rod Model: Weak Formulation

**State Space:**  $\xi(t) = (u(t, \cdot), u(t, \ell))$  in

$$X = L^2(0, \ell) \times \mathbb{R}$$

$$\langle \Phi_1, \Phi_2 \rangle_X = \int_0^\ell \rho A \phi_1 \phi_2 dx + m_\ell \varphi_1 \varphi_2$$

**Space of Test Functions:**

$$V = \{ \Phi = (\phi, \varphi) \in X \mid \phi \in H^1(0, \ell), \phi(0) = 0, \phi(\ell) = \varphi \}$$

$$\langle \Phi_1, \Phi_2 \rangle_V = \int_0^\ell Y A \phi_1' \phi_2' dx + k_\ell \varphi_1 \varphi_2$$

**Integration by Parts:**

$$\int_0^\ell \rho A \frac{\partial^2 u}{\partial t^2} \phi dx + \int_0^\ell N \frac{d\phi}{dx} dx - N(t, \ell) \phi(\ell) = \int_0^\ell f \phi dx$$

# Rod Model: Weak Formulation

Model:

$$\begin{aligned} & \int_0^\ell \rho A \frac{\partial^2 u}{\partial t^2} \phi dx + \int_0^\ell \left[ Y A \frac{\partial u}{\partial x} + c A \frac{\partial^2 u}{\partial x \partial t} \right] \frac{d\phi}{dx} dx \\ &= \int_0^\ell f \phi dx + a_2 A M^2(t) \int_0^\ell \frac{d\phi}{dx} dx \\ & - \left[ k_\ell u(t, \ell) + c_\ell \frac{\partial u}{\partial t}(t, \ell) + m_\ell \frac{\partial^2 u}{\partial t^2}(t, \ell) \right] \phi(\ell) \end{aligned}$$

for all  $(\phi, \varphi) = (\phi, \phi(\ell)) \in V$

**Note:** For conservative case, weak formulation can also be derived using energy principles.

# Rod Model: Strong and Weak Formulations

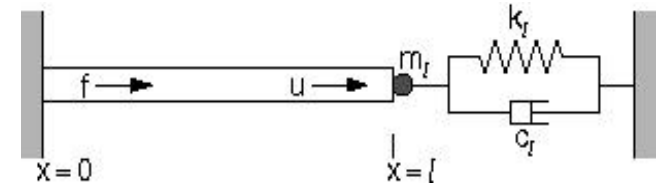
Rod Model:

$$\rho A \frac{\partial^2 u}{\partial t^2} - Y A \frac{\partial^2 u}{\partial x^2} - c A \frac{\partial^3 u}{\partial x^2 \partial t} = f$$

Boundary Conditions:

$$u(t, 0) = 0$$

$$N(t, \ell) = -k_\ell u(t, \ell) - c_\ell \frac{\partial u}{\partial t}(t, \ell) - m_\ell \frac{\partial^2 u}{\partial t^2}(t, \ell)$$



Weak Formulation:

$$\int_0^\ell \rho A \frac{\partial^2 u}{\partial t^2} \phi dx + \int_0^\ell \left[ Y A \frac{\partial u}{\partial x} + c A \frac{\partial^2 u}{\partial x \partial t} \right] \frac{d\phi}{dx} dx$$

$$= \int_0^\ell f \phi dx - \left[ k_\ell u(t, \ell) + c_\ell \frac{\partial u}{\partial t}(t, \ell) + m_\ell \frac{\partial^2 u}{\partial t^2}(t, \ell) \right] \phi(\ell)$$

for all  $(\phi, \varphi) = (\phi, \phi(\ell)) \in V$



## Weak Formulation: Energy Principles

**Issues:** Need conservative problem; take  $c = f = k_\ell = c_\ell = m_\ell = 0$

**Kinetic Energy:** 
$$K = \frac{1}{2} \int_0^L \rho A u_t^2(t, x) dx$$

**Potential Energy:** 
$$U = \frac{1}{2} \int_0^L N \varepsilon dx = \frac{1}{2} \int_0^L \sigma A \varepsilon dx = \frac{1}{2} \int_0^L Y A u_x^2(t, x) dx$$

# Weak Formulation: Energy Principles

'Action' Integral:

$$\mathcal{A}[u] = \int_{t_0}^{t_1} \mathcal{L} dt$$

where

$$\mathcal{L} = \frac{1}{2} \int_0^L [\rho A u_t^2 - Y A u_x^2] dx$$

Hamilton's Principle:

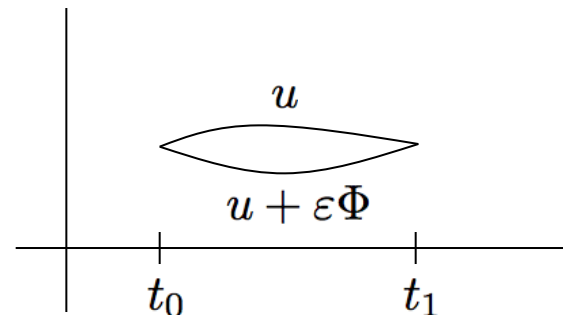
$$\delta \mathcal{A}[u; \Phi] = \frac{d}{d\varepsilon} \mathcal{A}[u + \varepsilon \Phi] \Big|_{\varepsilon=0} = 0$$

Admissible variations:

$$\hat{u}(t, x) = u(t, x) + \varepsilon \eta(t) \phi(x)$$

where

- (i)  $\eta(t_0) = \eta(t_1) = 0$
- (ii)  $\phi \in V = H_0^1(0, L)$



# Weak Formulation: Energy Principles

Hamilton's Principle:

$$\begin{aligned}\frac{d}{d\varepsilon} \mathcal{A}[u + \varepsilon\Phi] \Big|_{\varepsilon=0} &= \frac{1}{2} \frac{d}{d\varepsilon} \int_{t_0}^{t_1} \int_0^L [\rho A (u_t + \varepsilon \dot{\eta}\phi)^2 - Y A (u_x + \varepsilon \eta\phi')^2] dx dt \Big|_{\varepsilon=0} \\ &= \int_{t_0}^{t_1} \int_0^L [\rho A (u_t + \varepsilon \dot{\eta}\phi) \dot{\eta}\phi - Y A (u_x + \varepsilon \eta\phi') \eta\phi'] dx dt \Big|_{\varepsilon=0} \\ &= \int_{t_0}^{t_1} \int_0^L [\rho A u_t \dot{\eta}\phi - Y A u_x \eta\phi'] dx dt \\ &= - \int_{t_0}^{t_1} \eta(t) \int_0^L [\rho A u_{tt}\phi + Y A u_x \phi'] dx dt\end{aligned}$$

Weak Formulation:

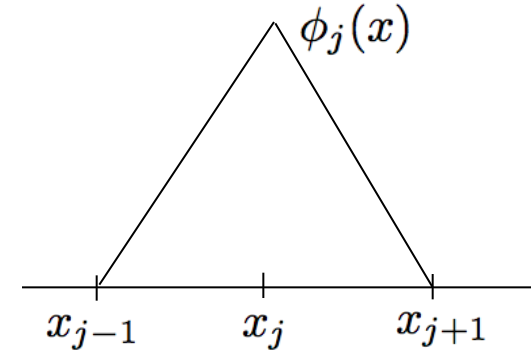
$$\int_0^L \rho A u_{tt}\phi dx + Y A \int_0^L u_x \phi' dx = 0 \quad \text{for all } \phi \in V$$

**Note:** Use integration by parts to show equivalence to strong formulation

# Approximation Techniques for the Rod Model: Galerkin

Linear Basis:

$$\phi_j(x) = \frac{1}{h} \begin{cases} x - x_{j-1}, & x_{j-1} \leq x < x_j \\ x_{j+1} - x, & x_j \leq x \leq x_{j+1} \\ 0, & \text{otherwise} \end{cases}$$



Approximate Solution:

$$u^N(t, x) = \sum_{j=1}^N u_j(t) \phi_j(x)$$

System:

$$\begin{aligned} \sum_{j=1}^N \ddot{u}_j(t) \int_0^\ell \rho A \phi_i \phi_j dx + \sum_{j=1}^N \dot{u}_j(t) \int_0^\ell c A \phi_i' \phi_j' dx + \sum_{j=1}^N u_j(t) \int_0^\ell Y A \phi_i' \phi_j' dx \\ = \int_0^\ell f \phi_i dx - \left( k_\ell u_N(t) \phi_N(\ell) + c_\ell \dot{u}_N(t) \phi_N(\ell) + m_\ell \ddot{u}_N(t) \phi_N(\ell) \right) \phi_N(\ell) \end{aligned}$$

for  $i = 1, \dots, N$

# Approximation Techniques for the Rod Model: Galerkin

## 2nd-Order Vector System:

$$\mathbb{M} \ddot{\mathbf{u}}(t) + \mathbb{Q} \dot{\mathbf{u}} + \mathbb{K} \mathbf{u}(t) = \mathbf{f}(t)$$

where  $\mathbf{u}(t) = [u_1(t), \dots, u_N(t)]^T$  and

$$[\mathbb{M}]_{ij} = \begin{cases} \int_0^\ell \rho A \phi_i \phi_j dx & , \quad i \neq N \text{ or } j \neq N \\ \int_0^\ell \rho A \phi_i \phi_j dx + m_\ell & , \quad i = N \text{ and } j = N \end{cases}$$

$$[\mathbb{K}]_{ij} = \begin{cases} \int_0^\ell Y A \phi_i' \phi_j' dx & , \quad i \neq N \text{ or } j \neq N \\ \int_0^\ell Y A \phi_i' \phi_j' dx + k_\ell & , \quad i = N \text{ and } j = N \end{cases}$$

$$[\mathbb{Q}]_{ij} = \begin{cases} \int_0^\ell c A \phi_i' \phi_j' dx & , \quad i \neq N \text{ or } j \neq N \\ \int_0^\ell c A \phi_i' \phi_j' dx + c_\ell & , \quad i = N \text{ and } j = N \end{cases}$$

$$[\mathbf{f}]_i = \int_0^\ell f \phi_i dx$$

# Approximation Techniques for the Rod Model: Galerkin

Matrices: Constant coefficients

$$\mathbb{M} = \rho Ah \begin{bmatrix} \frac{2}{3} & \frac{1}{6} & 0 & \cdots & 0 \\ \frac{1}{6} & \frac{2}{3} & \frac{1}{6} & & \\ & \ddots & \ddots & \ddots & \\ & & \frac{1}{6} & \frac{2}{3} & \frac{1}{6} \\ 0 & \cdots & 0 & \frac{1}{6} & \frac{1}{3} + \frac{m_\ell}{h} \end{bmatrix}, \quad \mathbb{K} = \frac{YA}{h} \begin{bmatrix} 2 & -1 & 0 & \cdots & 0 \\ -1 & 2 & -1 & & \\ & \ddots & \ddots & \ddots & \\ & & -1 & 2 & -1 \\ 0 & \cdots & 0 & -1 & 1 + hk_\ell \end{bmatrix}$$

First-Order System:

$$\dot{\mathbf{z}}(t) = \mathbb{A} \mathbf{z}(t) + \mathbf{F}(t)$$

$$\mathbf{z}(0) = \mathbf{z}_0$$

where

$$\mathbb{A} = \begin{bmatrix} 0 & \mathbb{I} \\ -\mathbb{M}^{-1}\mathbb{K} & -\mathbb{M}^{-1}\mathbb{Q} \end{bmatrix}, \quad \mathbf{F}(t) = \begin{bmatrix} 0 \\ \mathbb{M}^{-1}\mathbf{f}(t) \end{bmatrix}$$

Note: Codes available at [http://www4.ncsu.edu/~rsmith/Smart\\_Material\\_Systems/Chapter8/](http://www4.ncsu.edu/~rsmith/Smart_Material_Systems/Chapter8/)

# Approximation Techniques for the Rod Model: Finite Element

Motivating Problem:  $\rho A \frac{\partial^2 u}{\partial t^2} + Y A \frac{\partial^2 u}{\partial x^2} = 0$

Local Basis Elements: Take

$$\begin{aligned} u(t, x) &= a_0(t) + a_1(t)x \\ &= \boldsymbol{\varphi}^T(x) \mathbf{a}(t) \end{aligned}$$

where  $\mathbf{a}(t) = [a_0(t), a_1(t)]^T$  and  $\boldsymbol{\varphi}(x) = [1, x]^T$ . Then

$$\begin{bmatrix} u_\ell(t) \\ u_r(t) \end{bmatrix} = \begin{bmatrix} 1 & 0 \\ 1 & h \end{bmatrix} \begin{bmatrix} a_0(t) \\ a_1(t) \end{bmatrix}$$

$$\Rightarrow \mathbf{u}(t) = \mathbb{T} \mathbf{a}(t)$$

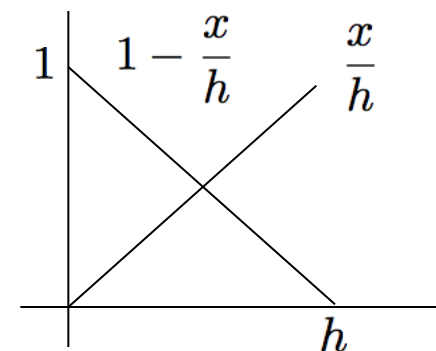
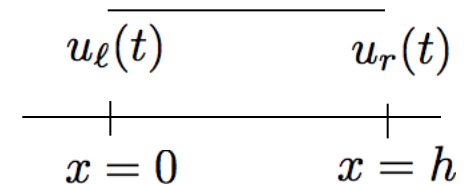
By observing that  $\mathbf{a}(t) = \mathbb{S} \mathbf{u}(t)$ , where

$$\mathbb{S} = \mathbb{T}^{-1} = \begin{bmatrix} 1 & 0 \\ -\frac{1}{h} & \frac{1}{h} \end{bmatrix},$$

it follows that displacements can be represented as

$$u(t, x) = \boldsymbol{\phi}^T(x) \mathbf{u}(t)$$

where  $\boldsymbol{\phi}^T(x) = [1 - \frac{x}{h}, \frac{x}{h}]$ .



# Approximation Techniques for the Rod Model: Finite Element

'Action' Integral:

$$\begin{aligned} \mathcal{A} &= \int_{t_0}^{t_1} [K - U] dt && \text{K: Kinetic Energy} \\ &= \int_{t_0}^{t_1} \frac{1}{2} \int_0^h [\rho A u_t^2(t, x) - Y A u_x^2(t, x)] dx dt && \text{U: Potential Energy} \end{aligned}$$

Here

$$u_x^2(t, x) = \mathbf{u}^T(t) \mathbf{S}^T \mathbb{D}(x) \mathbf{S} \mathbf{u}(t), \quad u_t^2(t, x) = \dot{\mathbf{u}}^T(t) \mathbf{S}^T \mathbb{F}(x) \mathbf{S} \dot{\mathbf{u}}(t)$$

where

$$\mathbb{D}(x) = \boldsymbol{\varphi}_x(x) \boldsymbol{\varphi}_x^T(x) = \begin{bmatrix} 0 & 0 \\ 0 & 1 \end{bmatrix}, \quad \mathbb{F}(x) = \boldsymbol{\varphi}(x) \boldsymbol{\varphi}^T(x) = \begin{bmatrix} 1 & x \\ x & x^2 \end{bmatrix}$$

Thus

$$\mathcal{A}[\mathcal{U}] = \int_{t_0}^{t_1} \frac{1}{2} [\dot{\mathbf{u}}^T(t) \mathbb{M}_e \dot{\mathbf{u}}(t) - \mathbf{u}^T(t) \mathbb{K}_e \mathbf{u}(t)] dt$$

where  $\mathcal{U} = (\mathbf{u}, \dot{\mathbf{u}})$  and

$$\begin{aligned} \mathbb{M}_e &= \rho A \mathbf{S}^T \cdot \int_0^h \mathbb{F}(x) dx \cdot \mathbf{S}, \quad \mathbb{K}_e = Y A \mathbf{S}^T \cdot \int_0^h \mathbb{D}(x) dx \cdot \mathbf{S} && \mathbb{M}_e: \text{Local Mass Matrix} \\ &&& \mathbb{K}_e: \text{Local Stiffness Matrix} \\ \Rightarrow \mathbb{M}_e &= \rho A h \begin{bmatrix} \frac{1}{3} & \frac{1}{6} \\ \frac{1}{6} & \frac{1}{3} \end{bmatrix}, \quad \mathbb{K}_e = \frac{Y A}{h} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \end{aligned}$$



# Approximation Techniques for the Rod Model: Finite Element

Hamilton's Principle: See "String and Membrane" lectures

$$\left. \frac{d}{d\varepsilon} \mathcal{A}[\mathcal{U} + \varepsilon \Upsilon] \right|_{\varepsilon=0} = 0$$

where  $\Upsilon = (\boldsymbol{\eta}, \dot{\boldsymbol{\eta}})$  and it is assumed that  $\boldsymbol{\eta}(t_0) = \boldsymbol{\eta}(t_1) = 0$ . Here

$$\mathcal{A}[\mathcal{U} + \varepsilon \Upsilon] = \int_{t_0}^{t_1} \frac{1}{2} \left[ (\dot{\mathbf{u}} + \varepsilon \dot{\boldsymbol{\eta}})^T \mathbb{M}_e (\dot{\mathbf{u}} + \varepsilon \dot{\boldsymbol{\eta}}) - (\mathbf{u} + \varepsilon \boldsymbol{\eta})^T \mathbb{K}_e (\mathbf{u} + \varepsilon \boldsymbol{\eta}) \right] dt$$

$$\Rightarrow \frac{d}{d\varepsilon} \mathcal{A}[\mathcal{U} + \varepsilon \Upsilon] = \int_{t_0}^{t_1} \frac{1}{2} \left[ \dot{\boldsymbol{\eta}}^T \mathbb{M}_e (\dot{\mathbf{u}} + \varepsilon \dot{\boldsymbol{\eta}}) + (\dot{\mathbf{u}} + \varepsilon \dot{\boldsymbol{\eta}})^T \mathbb{M}_e \dot{\boldsymbol{\eta}} \right. \\ \left. - \boldsymbol{\eta}^T \mathbb{K}_e (\mathbf{u} + \varepsilon \boldsymbol{\eta}) + (\mathbf{u} + \varepsilon \boldsymbol{\eta})^T \mathbb{K}_e \boldsymbol{\eta} \right] dt$$

$$\Rightarrow \left. \frac{d}{d\varepsilon} \mathcal{A}[\mathcal{U} + \varepsilon \Upsilon] \right|_{\varepsilon=0} = \int_{t_0}^{t_1} [\dot{\boldsymbol{\eta}}^T \mathbb{M}_e \dot{\mathbf{u}} - \boldsymbol{\eta}^T \mathbb{K}_e \mathbf{u}] dt \quad (\text{since } \dot{\mathbf{u}}^T \mathbb{M}_e \dot{\boldsymbol{\eta}} = \dot{\boldsymbol{\eta}}^T \mathbb{M}_e \dot{\mathbf{u}}) \\ = - \int_{t_0}^{t_1} \boldsymbol{\eta} [\mathbb{M}_e \ddot{\mathbf{u}} + \mathbb{K}_e \mathbf{u}] dt \quad (\text{integration by parts})$$

Local System:

$$\mathbb{M}_e \ddot{\mathbf{u}}(t) + \mathbb{K}_e \mathbf{u} = 0$$

# Approximation Techniques for the Rod Model: Finite Element

**Global Matrices:** Consider two subregions so  $h = \frac{\ell}{2}$ . Here

$$\mathbf{u}(t) = [u_{1\ell}(t), u_{2\ell}(t), u_{2r}(t)]^T$$

and

$$\mathbb{M} \ddot{\mathbf{u}} + \mathbb{K} \mathbf{u} = 0$$

where

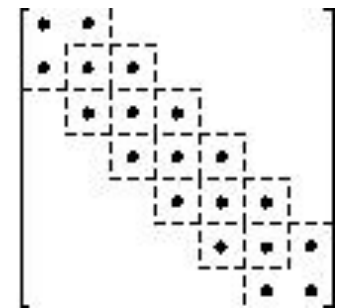
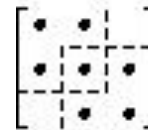
$$\mathbb{M} = \rho Ah \begin{bmatrix} \frac{1}{3} & \frac{1}{6} & 0 \\ \frac{1}{6} & \frac{2}{3} & \frac{1}{6} \\ 0 & \frac{1}{6} & \frac{1}{3} \end{bmatrix}, \quad \mathbb{K} = \frac{YA}{h} \begin{bmatrix} 1 & -1 & 0 \\ -1 & 2 & -1 \\ 0 & -1 & 1 \end{bmatrix}.$$

**Note:** Second row obtained by summing

$$\rho Ah \left( \frac{1}{6} \ddot{u}_{1\ell} + \frac{1}{3} \ddot{u}_{2\ell} \right) + \frac{YA}{h} (-u_{1\ell} + u_{2\ell}) = 0$$

$$\rho Ah \left( \frac{1}{3} \ddot{u}_{2\ell} + \frac{1}{6} \ddot{u}_{2r} \right) + \frac{YA}{h} (u_{2\ell} - u_{2r}) = 0$$

after enforcing  $u_{1r} = u_{2\ell}$  and  $\ddot{u}_{1r} = \ddot{u}_{2\ell}$ .



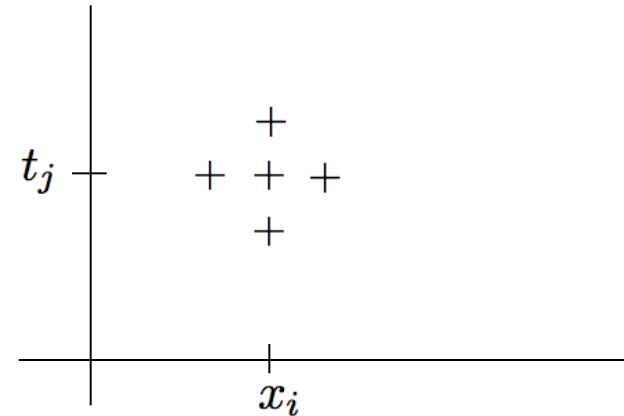
# Finite Difference Techniques for the Rod Model

Consider first

$$u_{tt} - K^2 u_{xx} = F$$

$$u(t, 0) = u(t, \ell) = 0$$

$$u(0, x) = f(x), \quad u_t(0, x) = g(x)$$



Grid:  $\Delta = \{(x_i, t_j) \mid x_i = ih, t_j = jk\}$

System:  $m = K \frac{k}{h}$

$$\frac{1}{k^2} [u_{i,j-1} - 2u_{i,j} + u_{i,j+1}] - \frac{K^2}{h^2} [u_{i-1,j} - 2u_{i,j} + u_{i+1,j}] = F(t_j, x_i)$$

$$\Rightarrow u_{i,j+1} = m^2 [u_{i+1,j} + u_{i-1,j}] + 2(1 - m^2)u_{i,j} - u_{i,j-1} + k^2 F(t_j, x_i)$$

Initial Conditions:

$$g(x_i) \approx \frac{u_{i,1} - u_{i,-1}}{2k} \Rightarrow u_{i,-1} = u_{i,1} - 2kg(x_i)$$

$$\Rightarrow u_{i,1} = \frac{m^2}{2} [f(x_{i+1}) + f(x_{i-1})] + (1 - m^2)f(x_i) + kg(x_i) + \frac{k^2}{2} F(t_0, x_i)$$

# Finite Difference Techniques for the Rod Model

Now consider

$$u_{tt} - c^2 u_{xxt} - K^2 u_{xx} = F$$

$$u(t, 0) = u(t, \ell) = 0$$

$$u(0, x) = f(x), \quad u_t(0, x) = g(x)$$

**Question:** What is finite difference scheme?