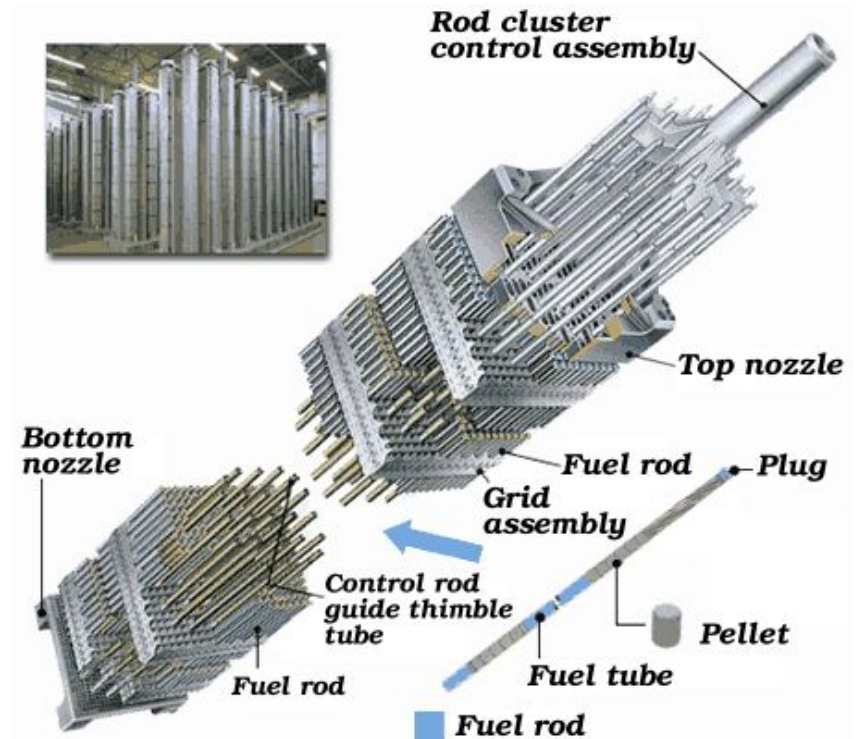
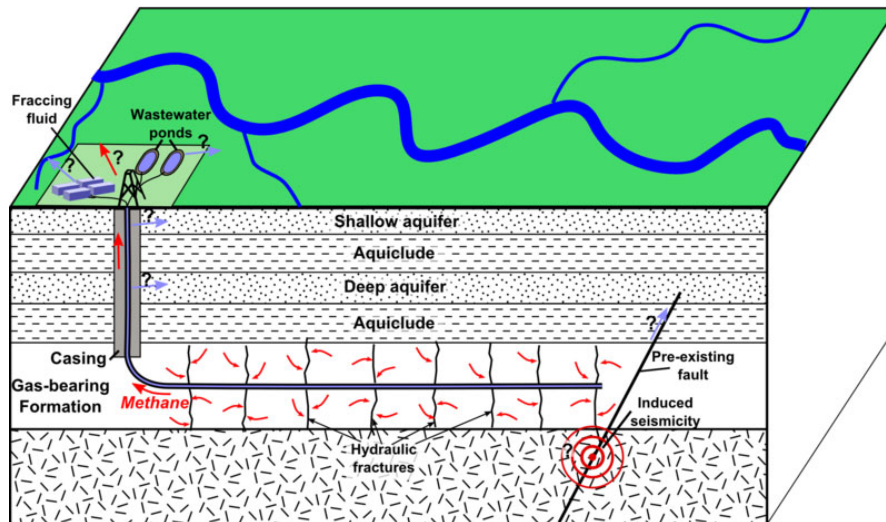
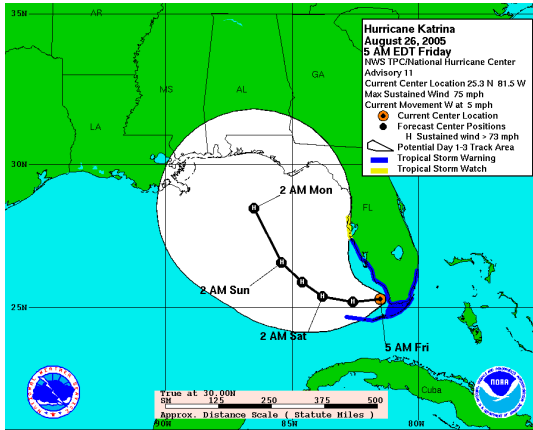


# Lecture 1: Motivation and Prototypical Examples

“Essentially all models are wrong, but some are useful,”

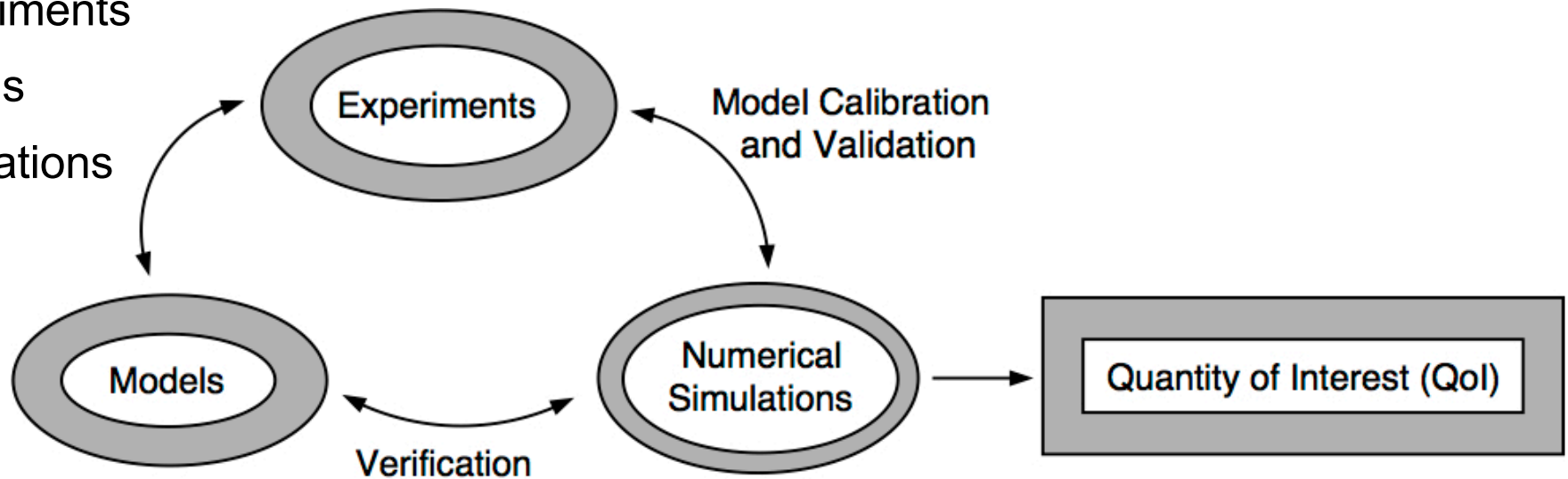
George E.P. Box, Industrial Statistician



# Predictive Science

**Components:** All involve uncertainty

- Experiments
- Models
- Simulations



- *Essentially, all models are wrong, but some are useful, George E.P. Box, Industrial Statistician.*
- *Computational results are believed by no one, except the person who wrote the code, source anonymous, quoted by Max Gunzburger, Florida State University.*
- *Experimental results are believed by everyone, except for the person who ran the experiment, source anonymous, quoted by Max Gunzburger, Florida State University.*
- *I have always done uncertainty quantification. The difference now is that it is capitalized. Bill Browning, Applied Mathematics Incorporated.*

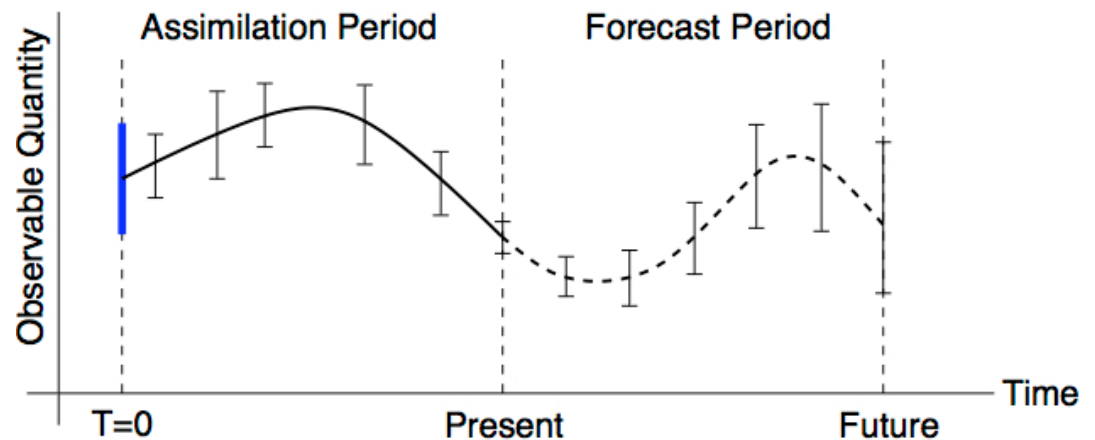
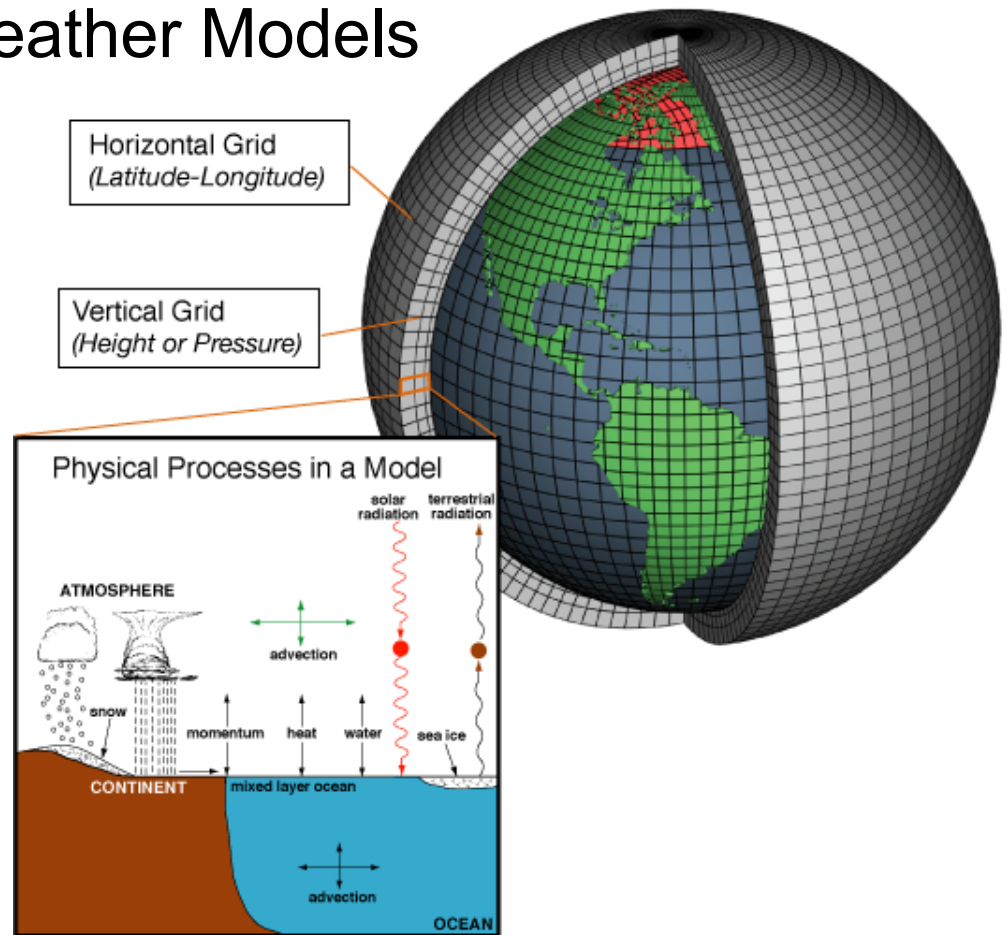
# Example 1: Weather Models

## Challenges:

- Coupling between temperature, pressure gradients, precipitation, aerosol, etc.;
- Models and inputs contain uncertainties;
- Numerical grids necessarily larger than many phenomena; e.g., clouds
- Sensors positions may be uncertain; e.g., weather balloons, ocean buoys.

## Goal:

- Assimilate data to quantify uncertain initial conditions and parameters;
- Make predictions with quantified uncertainties.



# Equations of Atmospheric Physics

Conservation Relations:

**Mass**  $\frac{\partial \rho}{\partial t} + \nabla \cdot (\rho v) = 0$

**Momentum**  $\frac{\partial v}{\partial t} = -v \cdot \nabla v - \frac{1}{\rho} \nabla p - g \hat{k} - 2\Omega \times v$

**Energy**  $\rho c_V \frac{\partial T}{\partial t} + p \nabla \cdot v = -\nabla \cdot F + \nabla \cdot (k \nabla T) + \rho \dot{q}(T, p, \rho)$

$p = \rho R T$

**Water**  $\frac{\partial m_j}{\partial t} = -v \cdot \nabla m_j + S_{m_j}(T, m_j, \chi_j, \rho), j = 1, 2, 3,$

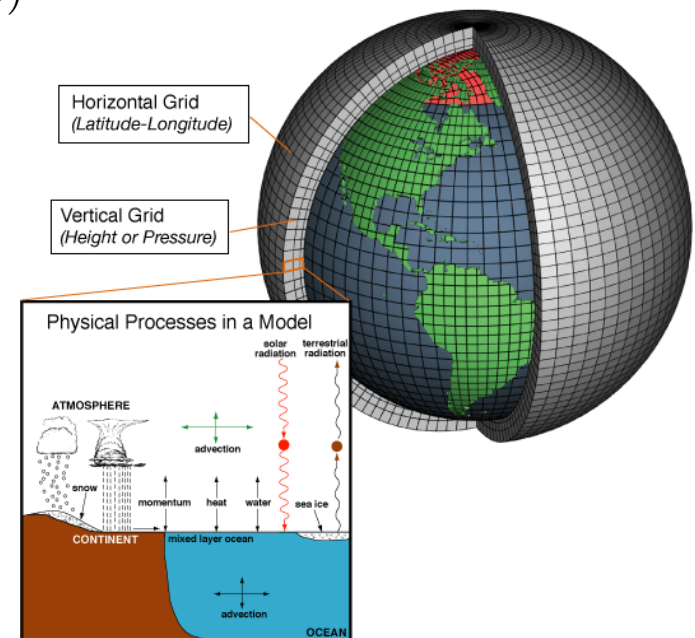
**Aerosol**  $\frac{\partial \chi_j}{\partial t} = -v \cdot \nabla \chi_j + S_{\chi_j}(T, \chi_j, \rho), j = 1, \dots, J,$

Constitutive Closure Relations: e.g.,

$$S_{m_2} = S_1 + S_2 + S_3 - S_4$$

where

$$S_1 = \bar{\rho} (m_2 - m_2^*)^2 \left[ \underline{1.2 \times 10^{-4}} + \left( \underline{1.569 \times 10^{-12}} \frac{n_r}{d_0 (m_2 - m_2^*)} \right) \right]^{-1}$$



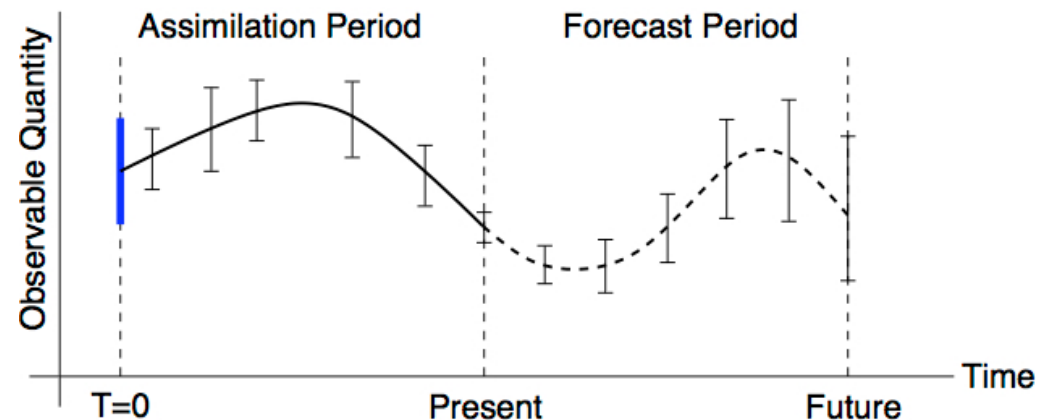
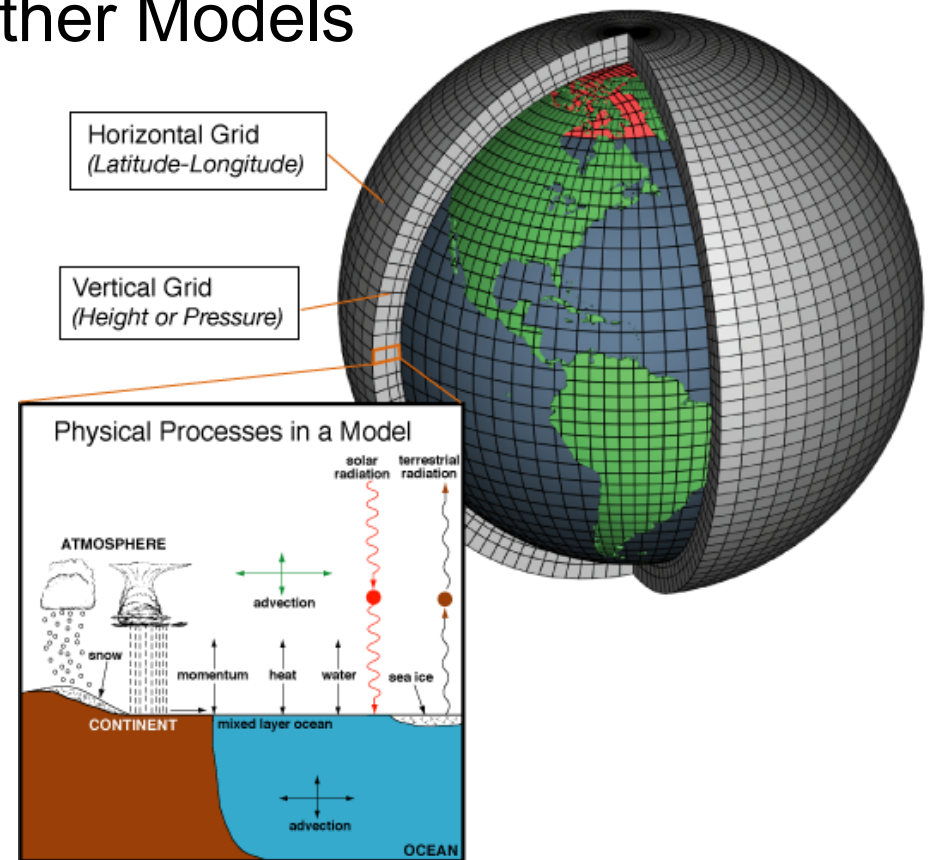
# Example 1: Weather Models

## Sources of Uncertainty:

- Model errors or discrepancies
- Input uncertainties
- Numerical errors and uncertainties
- Measurement errors and uncertainties

## Steps:

- Model Calibration: Involves the assimilation or integration of data to quantify and update input uncertainties.
- Model Prediction: Here one computes the response along with statistics, error bounds, or PDF; **extrapolation is important and difficult.**
- Estimation of the Validation Regime:
- **Goal:** Construct best estimate parameters and responses or quantities of interest with best estimate reduced uncertainties.



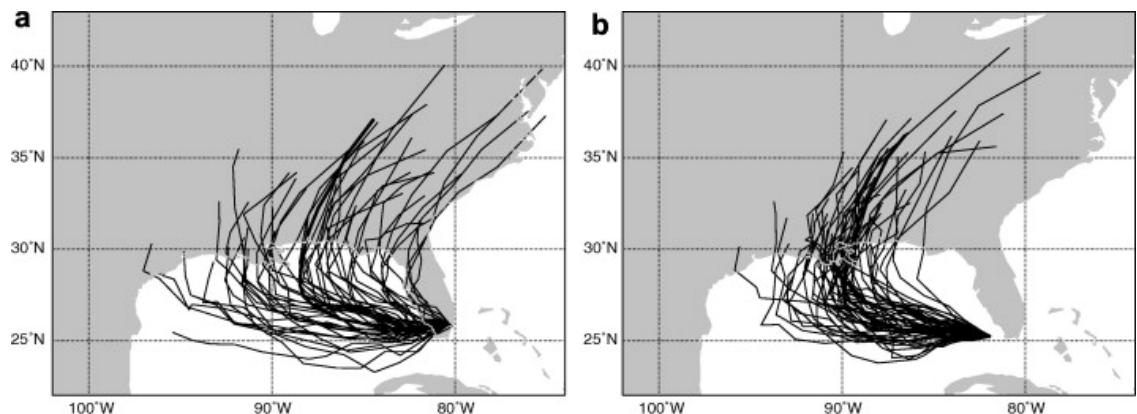
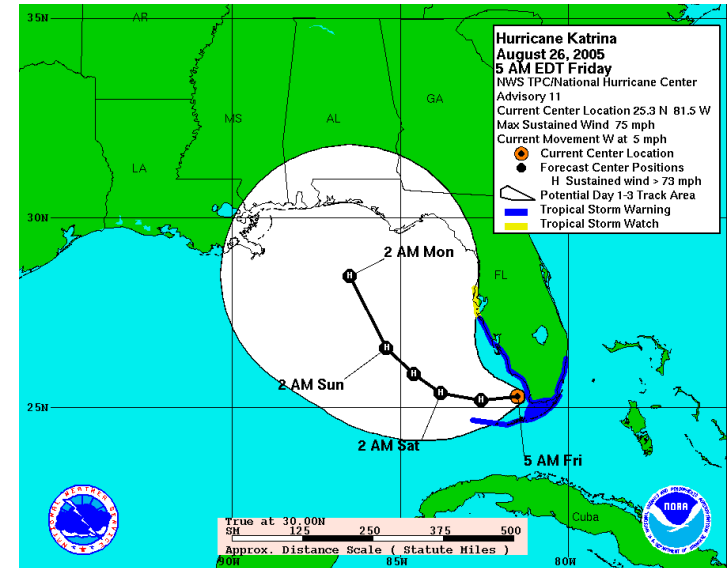
# Example 1: Weather Models

## Sources of Uncertainty:

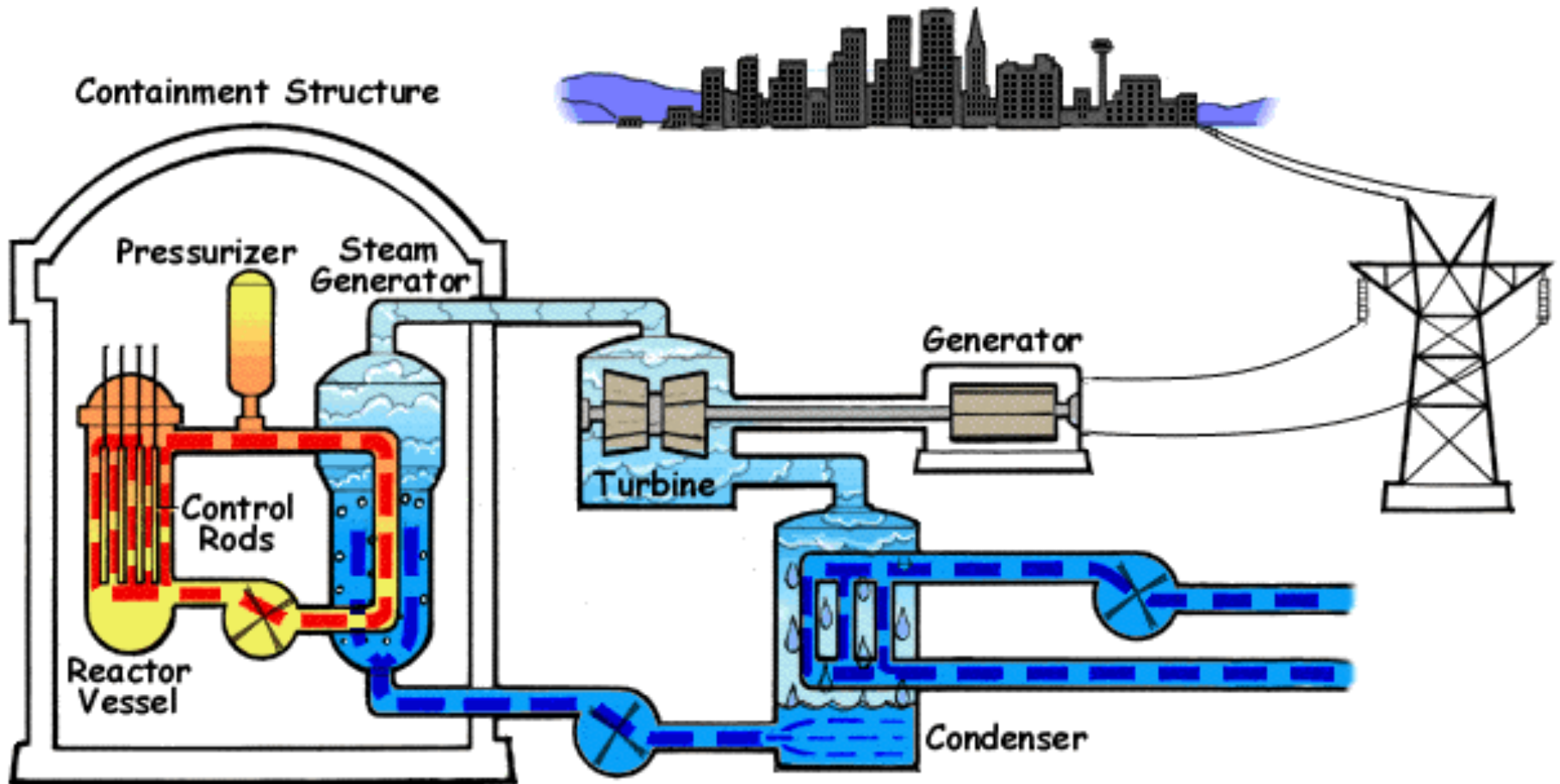
- Model errors or discrepancies
- Input uncertainties
- Numerical errors and uncertainties
- Measurement errors and uncertainties

## Ensemble Forecasts:

- Run multiple simulations with differing parameter values or initial conditions drawn from appropriate pdf.
- A 50% chance of rain means that given present atmospheric conditions, half of simulations predict measurable rain amount at random point in specified area.



## Example 2: Pressurized Water Reactors (PWR)



### Models:

- Involve neutron transport, thermal-hydraulics, chemistry.
- Inherently multi-scale, multi-physics.

**CRUD Measurements:** Consist of low resolution images at limited number of locations.

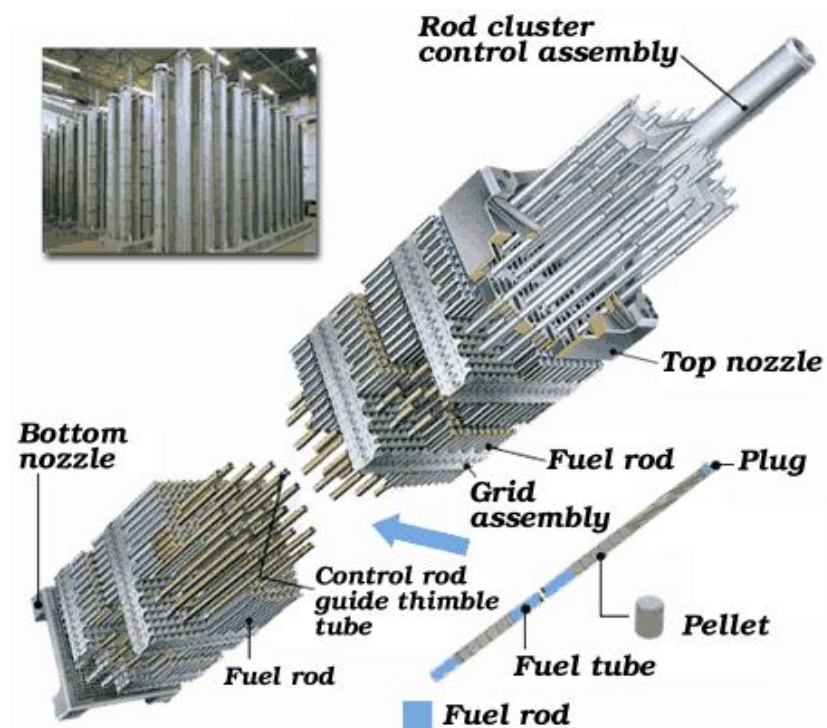
## Example 2: Pressurized Water Reactors (PWR)

### 3-D Neutron Transport Equations:

$$\begin{aligned} \frac{1}{|v|} \frac{\partial \varphi}{\partial t} + \Omega \cdot \nabla \varphi + \Sigma_t(r, E) \varphi(r, E, \Omega, t) \\ = \int_{4\pi} d\Omega' \int_0^\infty dE' \Sigma_s(E' \rightarrow E, \Omega' \rightarrow \Omega) \varphi(r, E', \Omega', t) \\ + \frac{\chi(E)}{4\pi} \int_{4\pi} d\Omega' \int_0^\infty dE' \nu(E') \Sigma_f(E') \varphi(r, E', \Omega', t) \end{aligned}$$

### Challenges:

- Linear in the state but function of 7 independent variables:  
 $r = x, y, z; E; \Omega = \theta, \phi; t$
- Very large number of inputs; e.g., 100,000;  
**Active subspace construction is critical.**
- ORNL Code SCALE: can take minutes to hours to run.
- SCALE TRITON has adjoint capabilities via TSUNAMI-2D and NEWT.





## Example 2: Pressurized Water Reactors (PWR)

**Thermo-Hydraulic Equations:** Mass, momentum and energy balance for fluid

$$\frac{\partial}{\partial t}(\alpha_f \rho_f) + \nabla \cdot (\alpha_f \rho_f v_f) = -\Gamma$$

$$\begin{aligned} \alpha_f \rho_f \frac{\partial v_f}{\partial t} + \alpha_f \rho_f v_f \cdot \nabla v_f + \nabla \cdot \sigma_f^R + \alpha_f \nabla \cdot \sigma + \alpha_f \nabla p_f \\ = -F^R - F + \Gamma(v_f - v_g)/2 + \alpha_f \rho_f g \end{aligned}$$

$$\begin{aligned} \frac{\partial}{\partial t}(\alpha_f \rho_f e_f) + \nabla \cdot (\alpha_f \rho_f e_f v_f + T h) &= (T_g - T_f)H + T_f \Delta_f \\ -T_g(H - \alpha_g \nabla \cdot h) + h \cdot \nabla T - \Gamma[e_f + T_f(s^* - s_f)] \\ -p_f \left( \frac{\partial \alpha_f}{\partial t} + \nabla \cdot (\alpha_f v_f) + \frac{\Gamma}{\rho_f} \right) \end{aligned}$$

**Note:** Similar equations for gas

### Codes:

- Low-Fidelity Code: COBRA-TF: Takes minutes to run
  - Sub-channel code -- cannot resolve between pins; no adjoint capabilities
- High-Fidelity Code: HYDRA: Takes hours to run
  - 3-D CFD code; no adjoint capabilities

## Example 2: Pressurized Water Reactors (PWR)

**Thermo-Hydraulic Equations:** Mass, momentum and energy balance for fluid

$$\frac{\partial}{\partial t}(\alpha_f \rho_f) + \nabla \cdot (\alpha_f \rho_f v_f) = -\Gamma$$

$$\begin{aligned} \alpha_f \rho_f \frac{\partial v_f}{\partial t} + \alpha_f \rho_f v_f \cdot \nabla v_f + \nabla \cdot \sigma_f^R + \alpha_f \nabla \cdot \sigma + \alpha_f \nabla p_f \\ = -F^R - F + \Gamma(v_f - v_g)/2 + \alpha_f \rho_f g \end{aligned}$$

$$\begin{aligned} \frac{\partial}{\partial t}(\alpha_f \rho_f e_f) + \nabla \cdot (\alpha_f \rho_f e_f v_f + Th) &= (T_g - T_f)H + T_f \Delta_f \\ -T_g(H - \alpha_g \nabla \cdot h) + h \cdot \nabla T - \Gamma[e_f + T_f(s^* - s_f)] \\ -p_f \left( \frac{\partial \alpha_f}{\partial t} + \nabla \cdot (\alpha_f v_f) + \frac{\Gamma}{\rho_f} \right) \end{aligned}$$

**Example:** Shearon Harris outside Raleigh



### UQ Questions:

- What is peak operating temperature?
- What is expected level of CRUD buildup?
- What is risk associated with operating regime?
- What is expected profit for new design?

# Example 3: HIV Model for Characterization/Treatment Regimes

**HIV Model:**  $\dot{T}_1 = \lambda_1 - d_1 T_1 - (1 - \varepsilon)k_1 V T_1$

**Notes:** 21 parameters

$$\dot{T}_2 = \lambda_2 - d_2 T_2 - (1 - f\varepsilon)k_2 V T_2$$

[Adams, Banks et al., 2005]

$$\dot{T}_1^* = (1 - \varepsilon)k_1 V T_1 - \delta T_1^* - m_1 E T_1^*$$

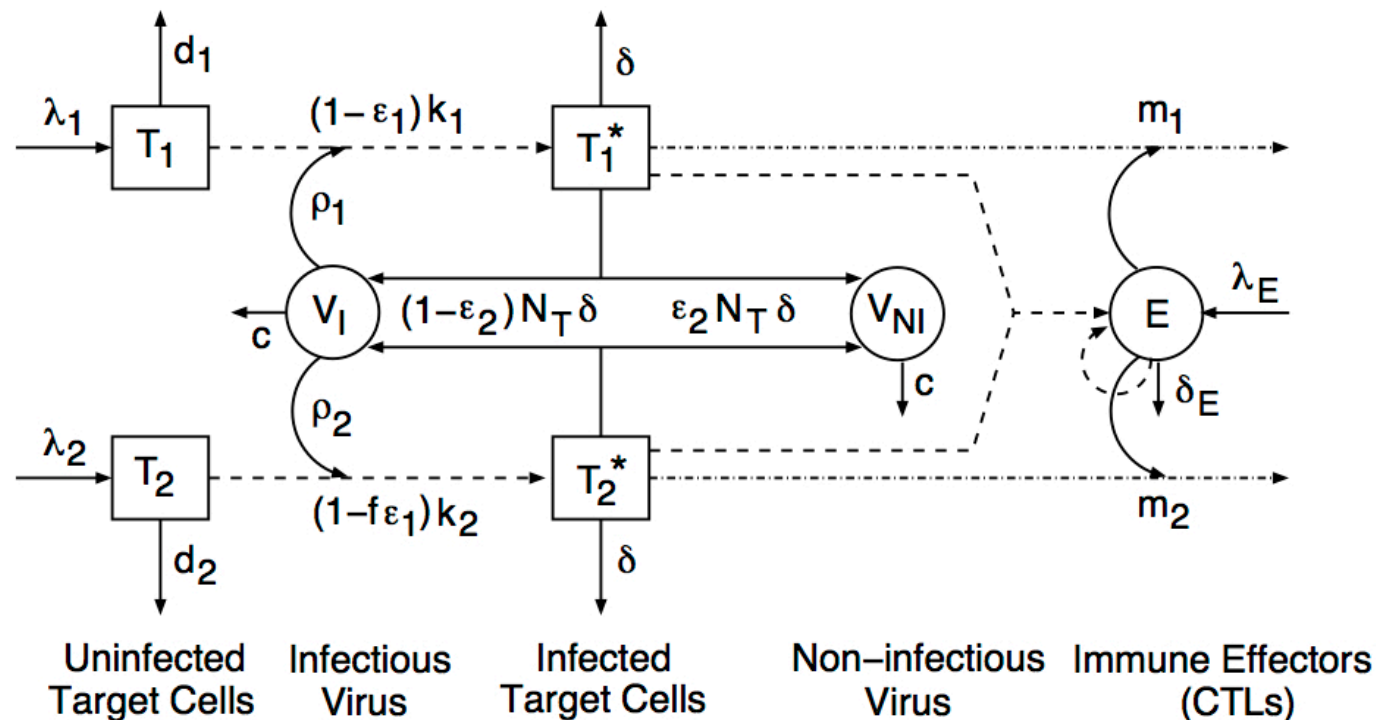
$$\dot{T}_2^* = (1 - f\varepsilon)k_2 V T_2 - \delta T_2^* - m_2 E T_2^*$$

$$\dot{V} = N_T \delta (T_1^* + T_2^*) - cV - [(1 - \varepsilon)\rho_1 k_1 T_1 + (1 - f\varepsilon)\rho_2 k_2 T_2]V$$

$$\dot{E} = \lambda_E + \frac{b_E (T_1^* + T_2^*)}{T_1^* + T_2^* + K_b} E - \frac{d_E (T_1^* + T_2^*)}{T_1^* + T_2^* + K_d} E - \delta_E E$$

**Notation:**  $\dot{E} \equiv \frac{dE}{dt}$

**Compartments:**



# Example 3: HIV Model for Characterization and Control Regimes

**HIV Model:** Used for characterization and control treatment regimes.

$$\dot{T}_1 = \lambda_1 - d_1 T_1 - (1 - \varepsilon) k_1 V T_1$$

$$\dot{T}_2 = \lambda_2 - d_2 T_2 - (1 - f\varepsilon) k_2 V T_2$$

$$\dot{T}_1^* = (1 - \varepsilon) k_1 V T_1 - \delta T_1^* - m_1 E T_1^*$$

$$\dot{T}_2^* = (1 - f\varepsilon) k_2 V T_2 - \delta T_2^* - m_2 E T_2^*$$

$$\dot{V} = N_T \delta (T_1^* + T_2^*) - cV - [(1 - \varepsilon) \rho_1 k_1 T_1 + (1 - f\varepsilon) \rho_2 k_2 T_2] V$$

$$\dot{E} = \lambda_E + \frac{b_E (T_1^* + T_2^*)}{T_1^* + T_2^* + K_b} E - \frac{d_E (T_1^* + T_2^*)}{T_1^* + T_2^* + K_d} E - \delta_E E$$

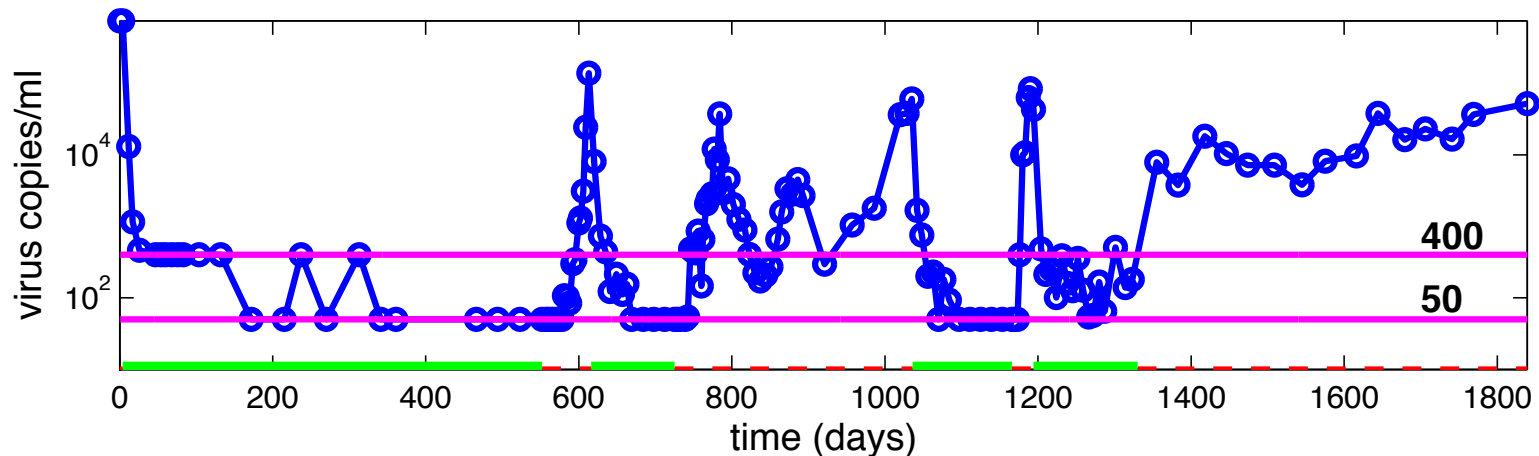
**Parameters:** Most are unknown and must be estimated from data

$\lambda_1$	Target cell 1 production rate	$\rho_1$	Ave. virions infecting type 1 cell
$\lambda_2$	Target cell 2 production rate	$\rho_2$	Ave. virions infecting type 2 cell
$d_1$	Target cell 1 death rate	$b_E$	Max. birth rate immune effectors
$d_2$	Target cell 2 death rate	$d_E$	Max. death rate immune effectors
$k_1$	Population 1 infection rate	$K_b$	Birth constant, immune effectors
$k_2$	Population 2 infection rate	$K_d$	Death constant, immune effectors
$c$	Virus natural death rate	$\lambda_E$	Immune effector production rate
$\delta$	Infected cell death rate	$\delta_E$	Natural death rate, immune effectors
$\varepsilon$	Population 1 treatment efficacy	$N_T$	Virions produced per infected cell
$m_1$	Population 1 clearance rate	$f$	Treatment efficacy reduction
$m_2$	Population 2 clearance rate		

# Example 3: HIV Model for Characterization and Control Regimes

**HIV Model:** Several sources of uncertainty including viral measurement techniques

**Example:** Upper and lower limits to assay sensitivity



## UQ Questions:

- What are the uncertainties in parameters that cannot be directly measured?
- What is expected viral load?
- What is optimal treatment regime that is “safe” for patient?

# Example 4: Portfolio Model

## Example: Portfolio model

$$Y = c_1 Q_1 + c_2 Q_2$$

### Note:

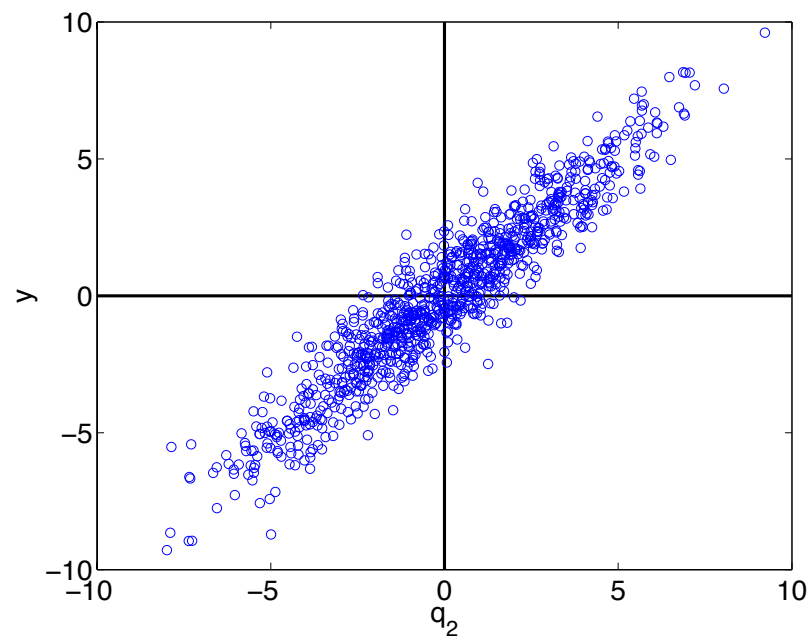
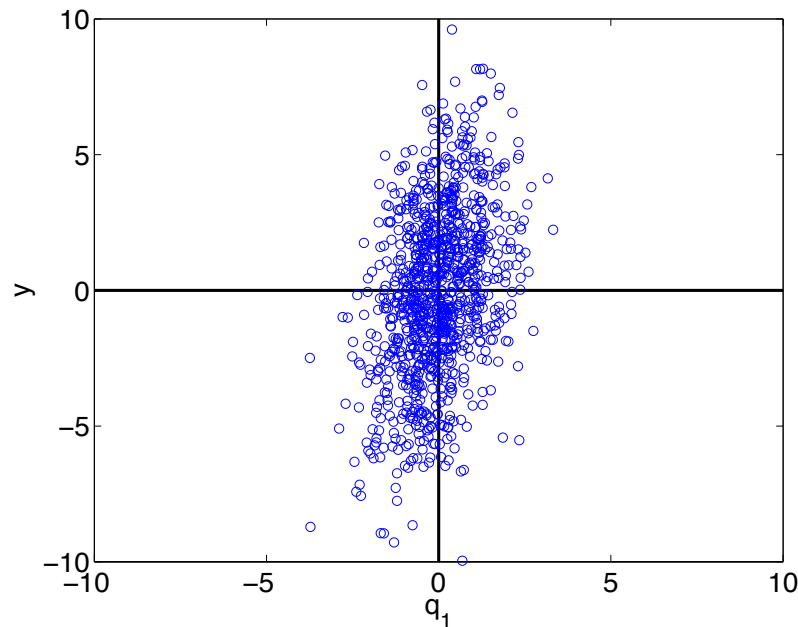
- $Q_1$  and  $Q_2$  represent hedged portfolios
- $c_1$  and  $c_2$  amounts invested in each portfolio

### Take

$$c_1 = 2, c_2 = 1$$

$$Q_1 \sim N(0, \sigma_1^2) \text{ with } \sigma_1 = 1$$

$$Q_2 \sim N(0, \sigma_2^2) \text{ with } \sigma_2 = 3$$



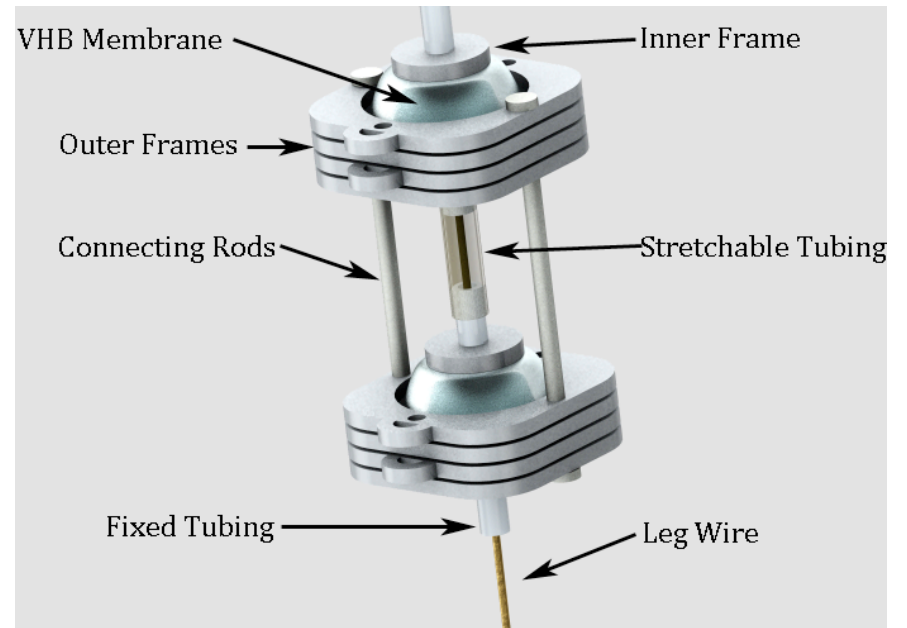
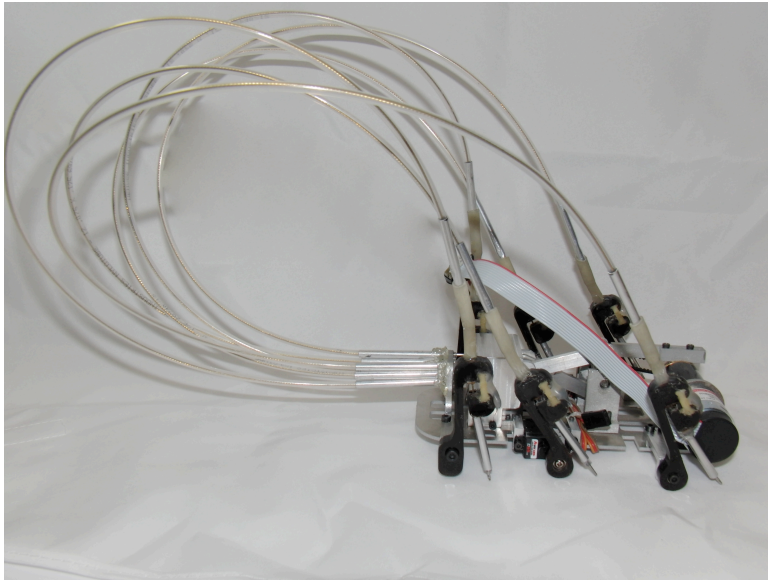
### UQ Questions:

- What is expected investment return?
- What is impact of market uncertainty on investment return?

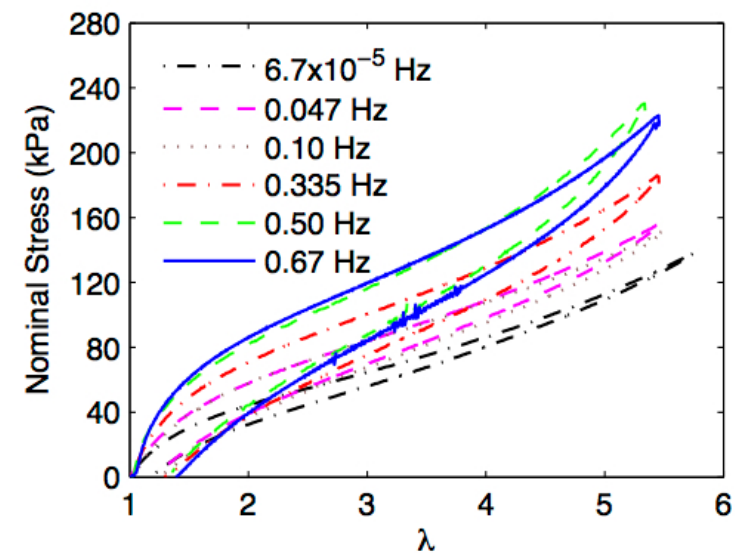
# Example 5: Viscoelastic Material Models

Application: Adaptive materials for legged robotics

- Figure: Billy Oates



Material Behavior: Significant rate dependence



# Example 5: Viscoelastic Material Models

Material Behavior: Significant rate dependence

Finite-Deformation Model:

- Nonlinear non-affine
- Hyperelastic energy function

$$\psi_{\infty}^N = \frac{1}{6} \underline{G_c} I_1 - \underline{G_c} \lambda_{\max}^2 \ln (3 \lambda_{\max}^2 - I_1) + \underline{G_e} \sum_j \left( \lambda_j + \frac{1}{\lambda_j} \right)$$

Parameters:

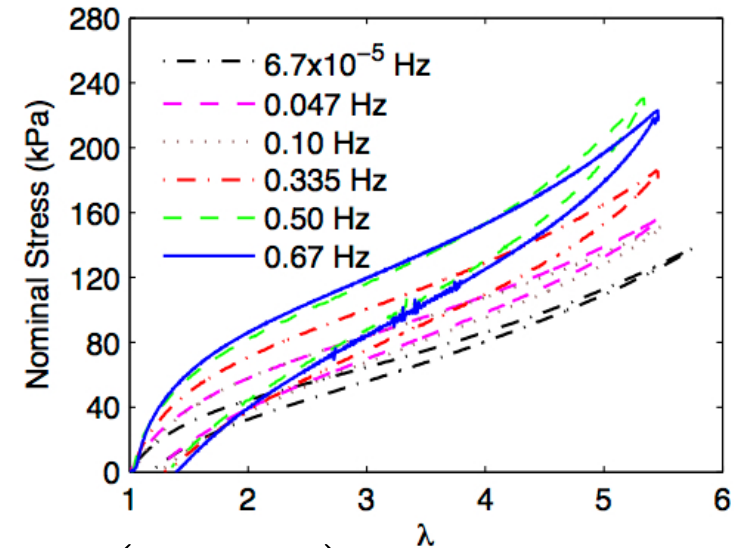
$$q = [G_e, G_c, \lambda_{\max}, \eta, \beta, \gamma]$$

$q = [\eta, \beta, \gamma]$ : Viscoelastic parameters

$G_c$ : Crosslink network modulus

$G_e$ : Plateau modulus

$\lambda_{\max}$ : Max stretch effective affine tube



Uncertainty Quantification Goals:

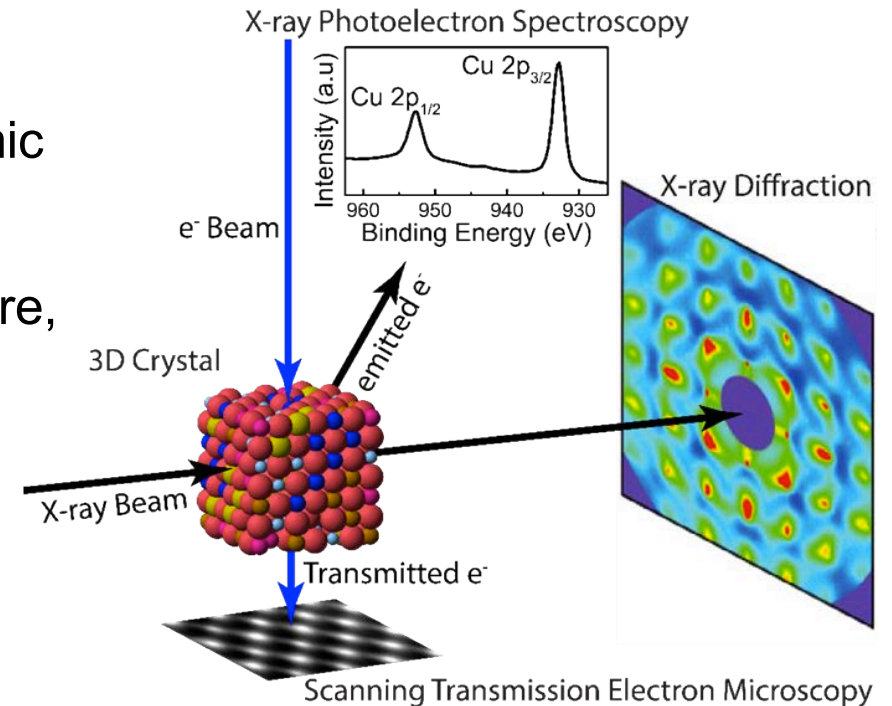
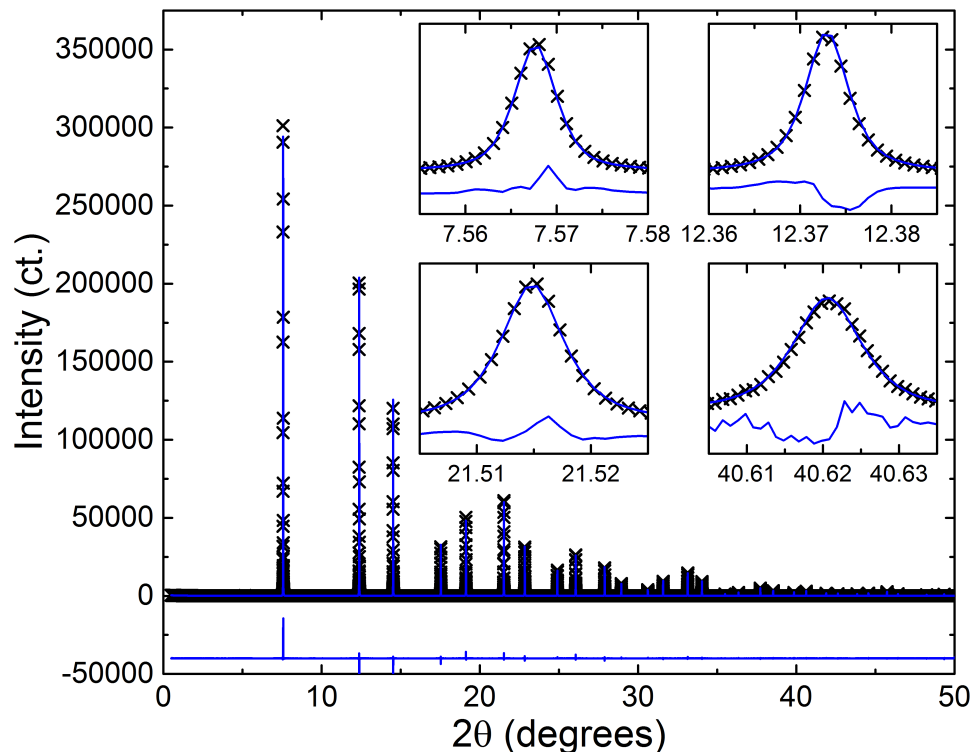
- Quantify measurement errors.
- Quantify uncertainty in parameters.
- Use statistics to quantify accuracy of considered models.



# Example 6: X-Ray Crystallography

## Properties:

- Reveal relative positions of atoms, their atomic number, types of chemical bonds, etc.
- Applications: determination of DNA structure, design of pharmaceuticals, etc..



## Uncertainty Quantification Goals:

- Use Bayesian analysis to quantify uncertainty associated with Rietveld model and background.
- Quantify heteroskedasticity and correlation of error structure.

Collaborators: Chris Fancher, Zhen Han, Igor Levin, Katherine Page, Brian Reich, Alyson Wilson, Jacob Jones

# Example 7: Quantum-Informed Continuum Models

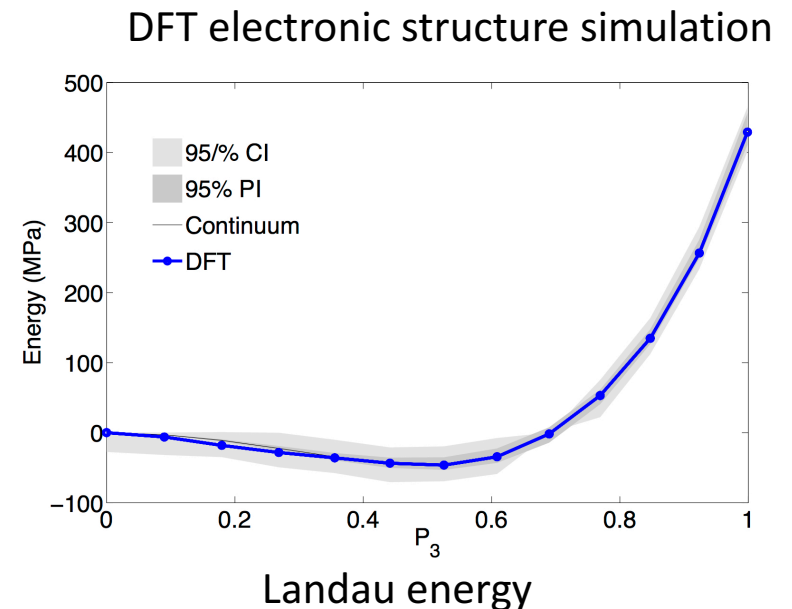
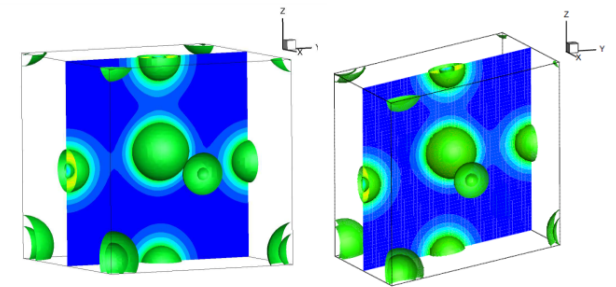
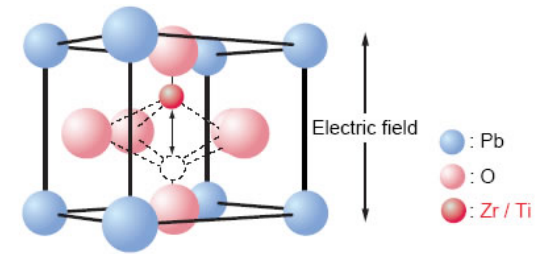
## Objectives:

- Compute energy about different strain states using density functional theory (DFT).
- Use DFT energy to calibrate Landau energy-based continuum models.

$$\Sigma = \Sigma(E_{IJ}, E_{IJ,K}, P_I, Q_{IJ}, \dots)$$

## UQ and Sensitivity Analysis Goals:

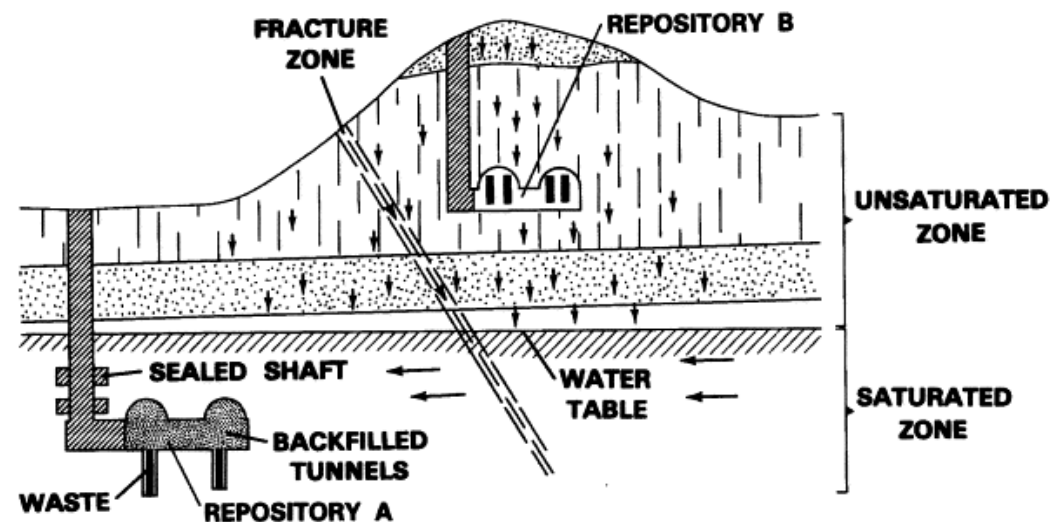
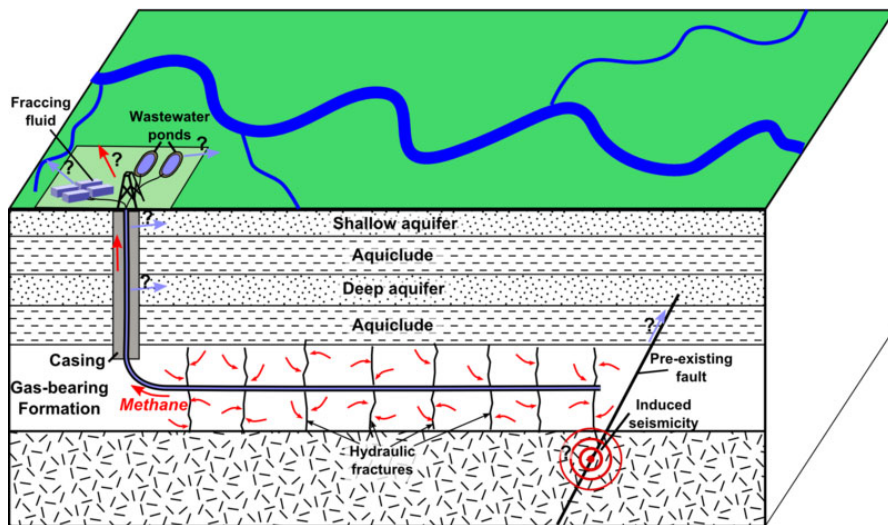
- Quantify uncertainty introduced when internal atomic and electronic degrees of freedom are neglected.
- Construct credible and prediction intervals to quantify accuracy of continuum models.
- Employ sensitivity analysis to determine influential model parameters.



# Experimental Uncertainties and Limitations

**Examples:** *Experimental results are believed by everyone, except for the person who ran the experiment, Max Gunzburger, Florida State University.*

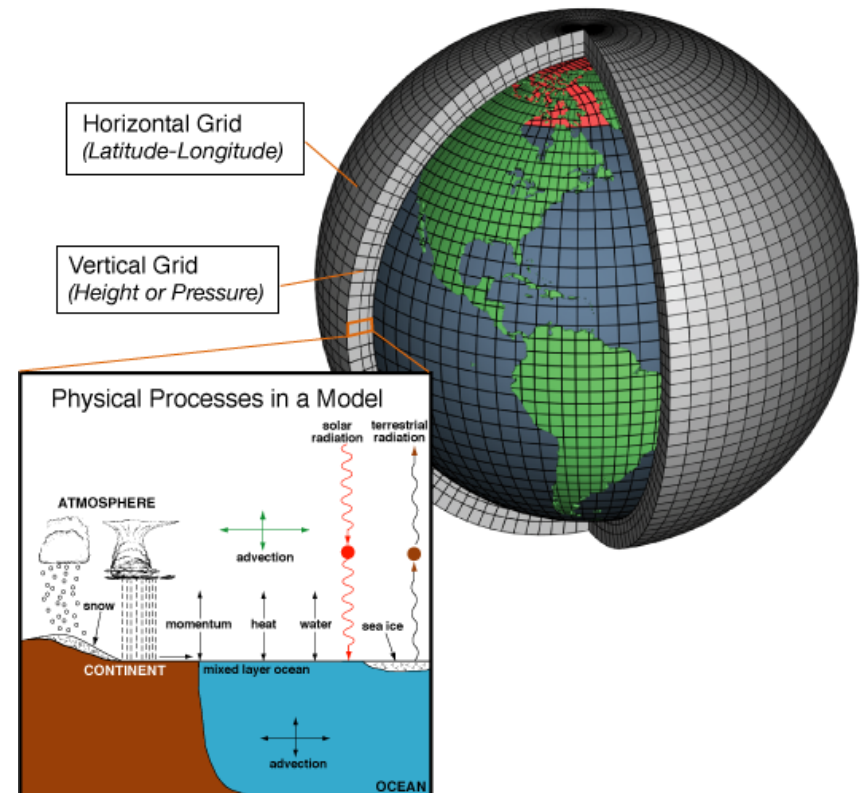
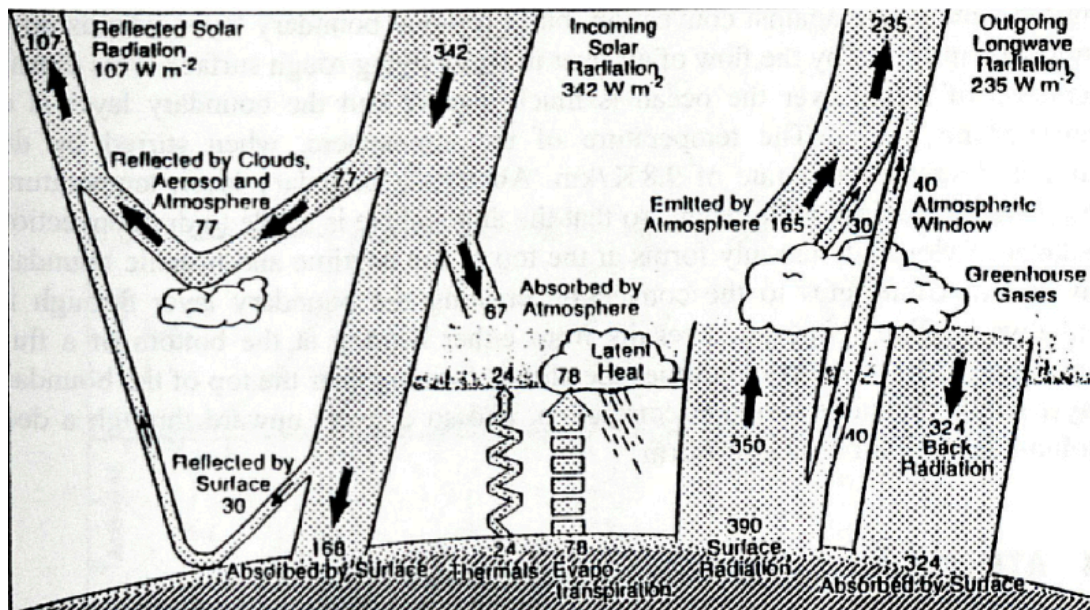
- Pharmaceutical and disease treatment strategies often too dangerous or expensive for human tests or large segments of the population.
- Climate scenarios cannot be experimentally tested at the planet scale. Instead, components such as volcanic forcing tested using measurements such as the 1991 Mount Pinatubo data.
- Subsurface hydrology data very limited due to infeasibility of drilling large numbers of wells. Result: significant uncertainty regarding subsurface structures.



# Model Errors

**Examples:** *Essentially, all models are wrong, but some are useful, George E.P. Box, Industrial Statistician*

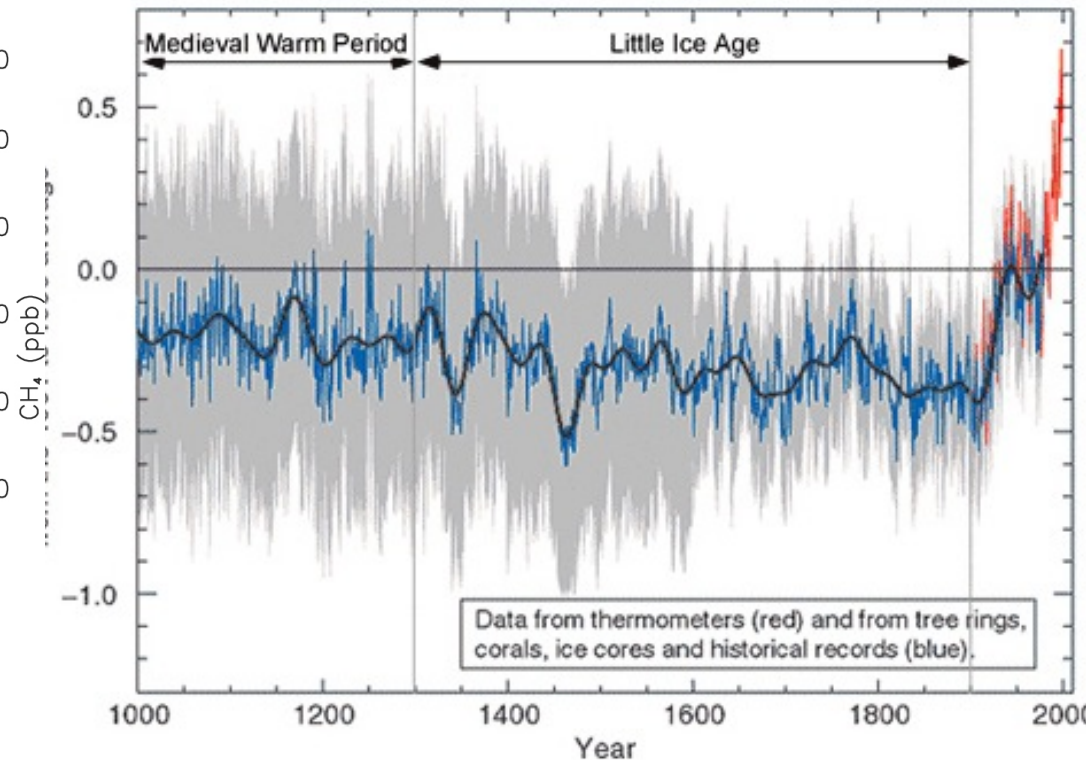
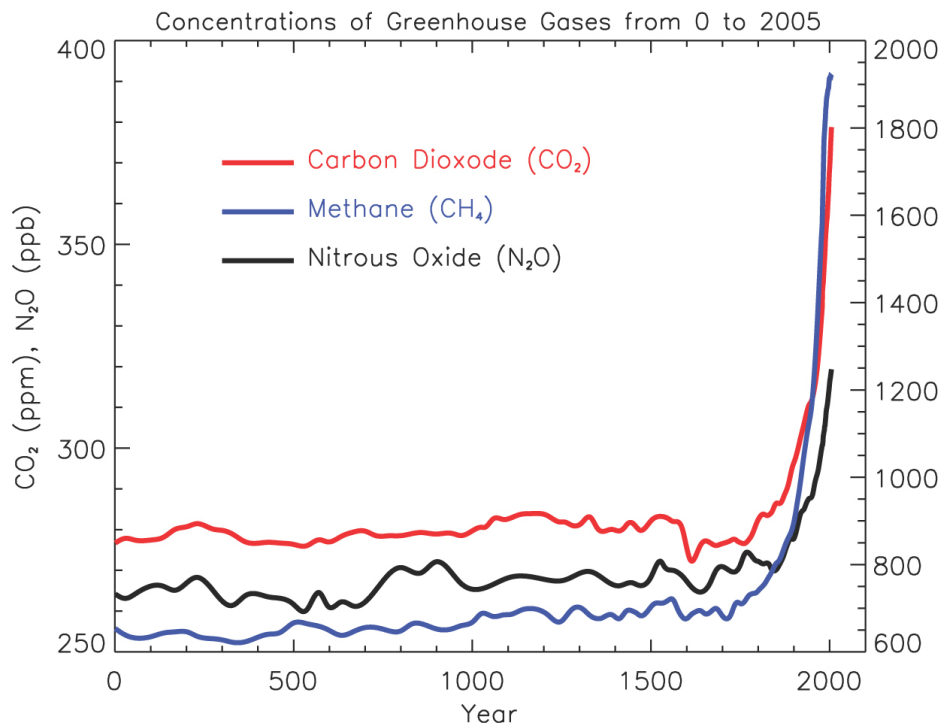
- Numerous components of weather and climate models --- e.g., aerosol-induced cloud formation, greenhouse gas processes --- occur on scales that are much smaller than numerical grids used to solve the atmospheric equations of physics. These processes represent highly complex physics that is only partially understood.
- Many biological applications are coupled, complex, highly nonlinear, and driven by poorly understood or stochastic processes.



# Input Uncertainties

**Note:** *Essentially, all models are wrong, but some are useful*, George E.P. Box, Industrial Statistician

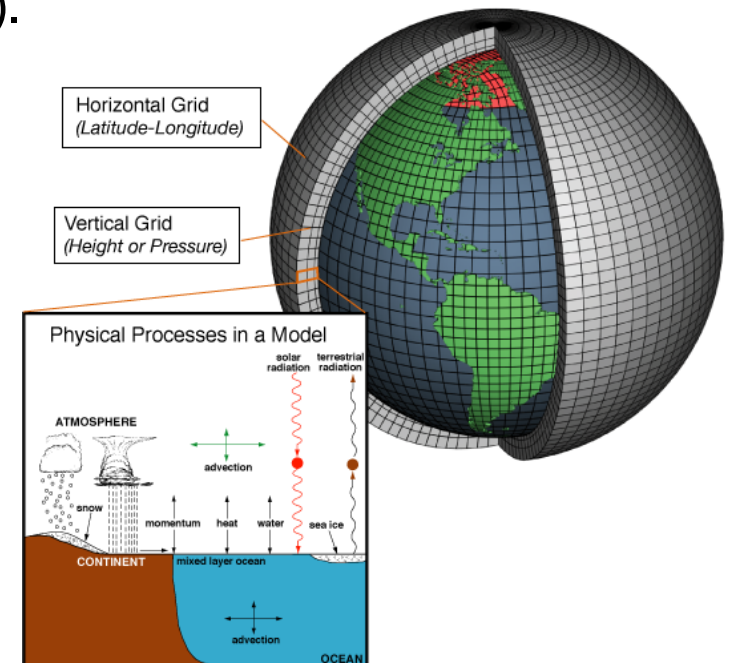
- Phenomenological models used to represent processes such as turbulence in weather, climate and nuclear reactor models have nonphysical parameters whose values and uncertainties must be determined using measured data.
- Forcing and feedback mechanisms in climate models serve as boundary inputs. These parameterized phenomenological relations introduce both model and parameter uncertainties.



# Numerical Errors

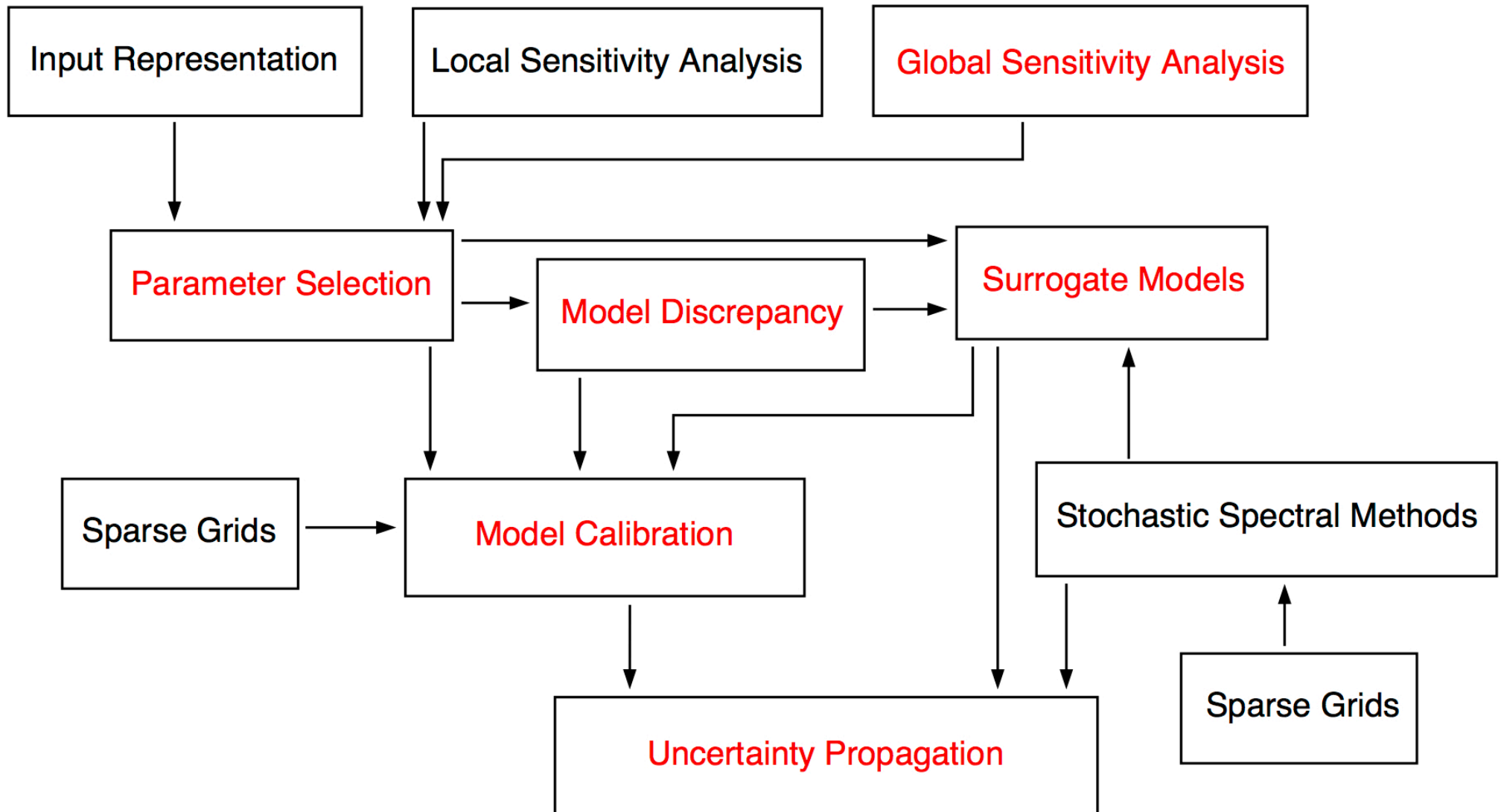
**Note:** *Computational results are believed by no one, except the person who wrote the code, Max Gunzburger, Florida State University.*

- Roundoff, discretization or approximation errors; e.g., mesh for nuclear subchannel code COBRA-TF is on the order of subchannel between rods.
- Bugs or coding errors;
- Bit-flipping, hardware failures and uncertainty associated with future exascale and quantum computing;
- Grids required for numerical solutions of field equations in applications such as weather or climate models (e.g., 50~km) are much larger than the scale of physics being modeled (e.g., turbulence or greenhouse gases).

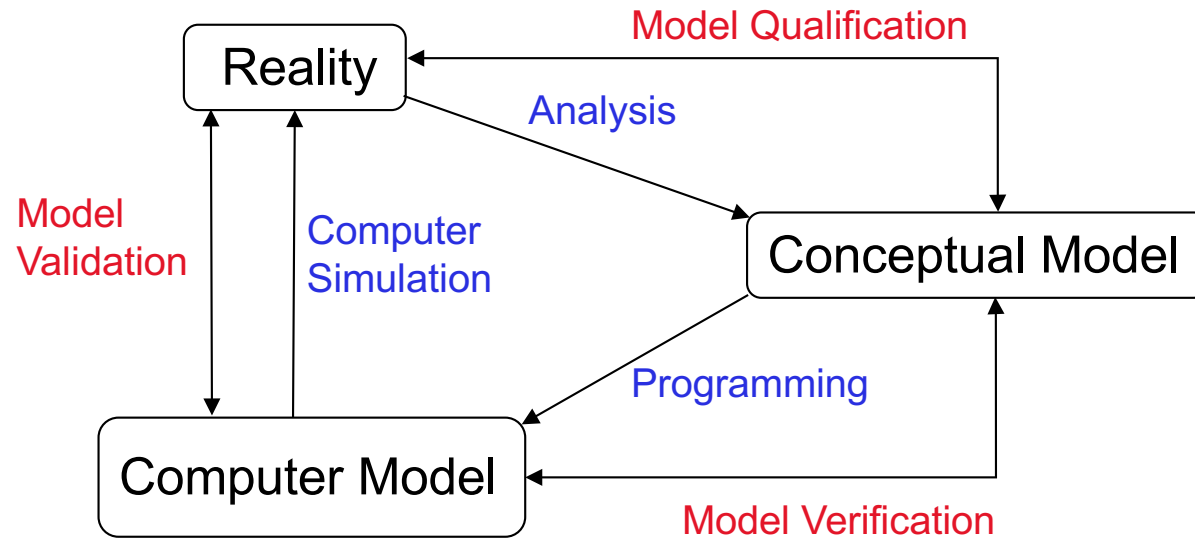


# Steps in Uncertainty Quantification

**Note:** Uncertainty quantification requires synergy between statistics, mathematics and application area.

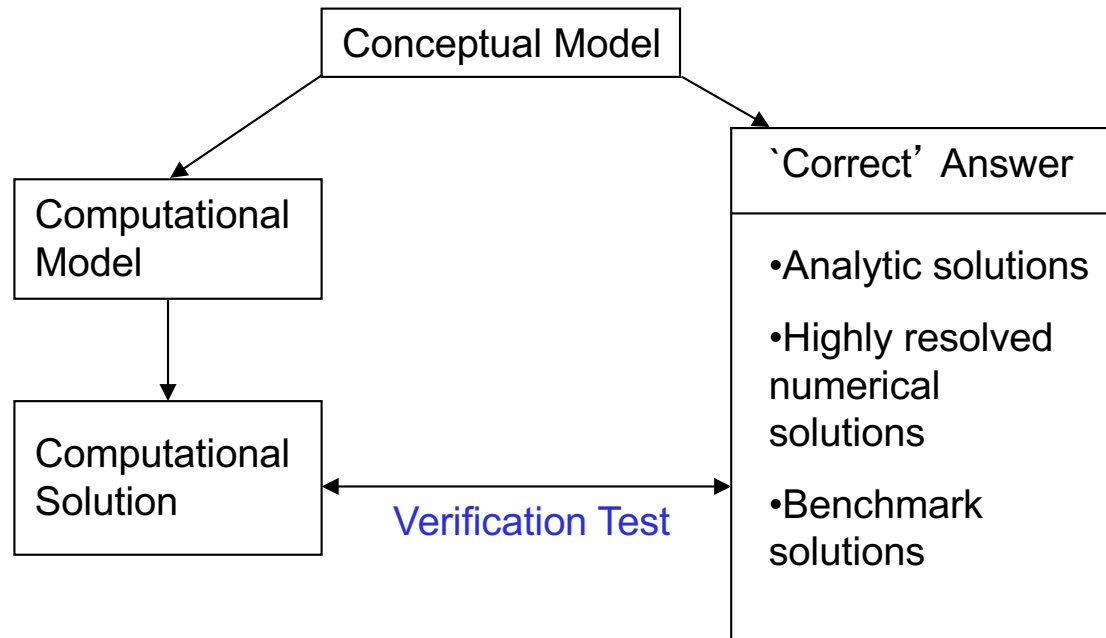


# Modeling Issues





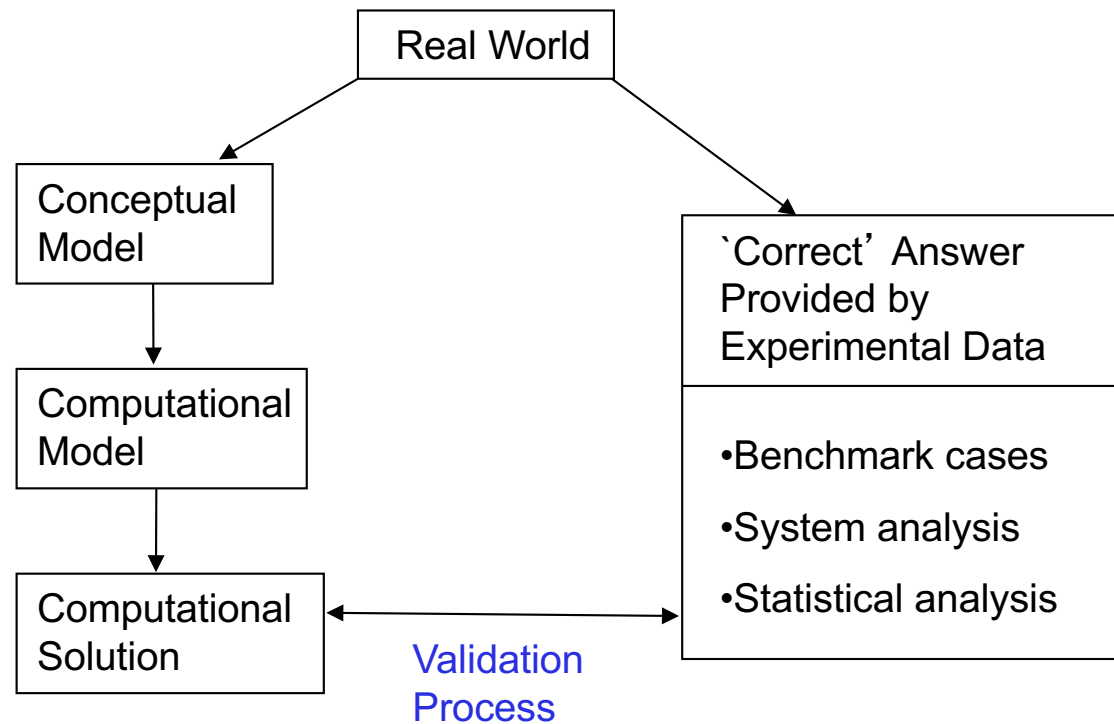
# Verification Process



**Verification:** The process of determining that a model implementation accurately represents the developer's conceptual description of the model and the solution to the model.

**Note:** Verification deals with mathematics

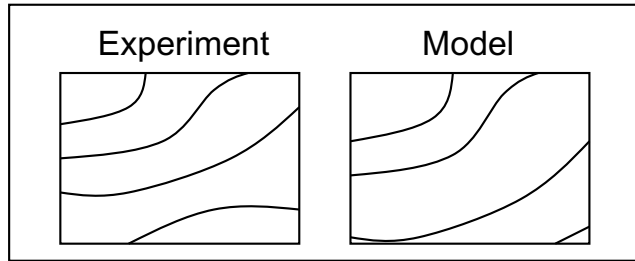
# Validation Process



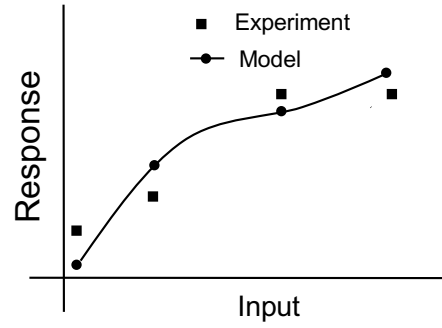
**Validation:** The process of determining the degree to which a model is an accurate representation of the real world from the perspective of the intended model users.

**Note:** Validation deals with physics and statistics

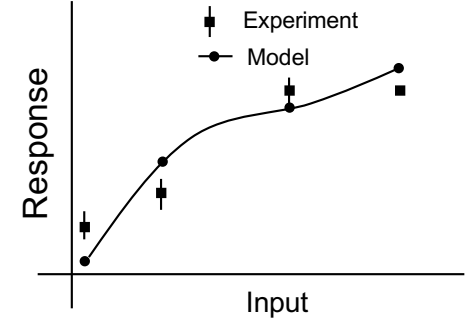
# Validation Metrics



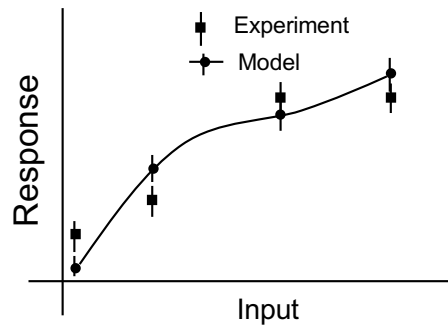
'Viewgraph' Norm



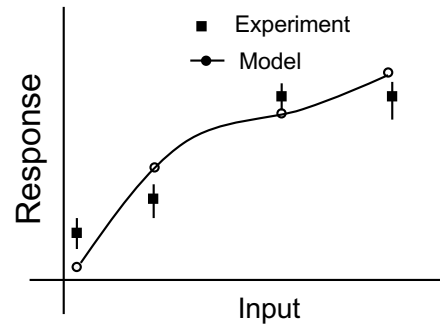
Deterministic



Experimental  
Uncertainty



Numerical Error



Nondeterministic  
Computation